



# The EMTO method

## Fundamentals, implementation and demonstration

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# Collaboration

**Hans L. Skriver (1998-2000)**

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# The EMTO theory

## Exact muffin-tin orbital theory

Andersen O. K., Jepsen O., Krier G.

1994

*in: Lectures on Methods of Electronic Structure Calculations, eds.: V. Kumar, O. K. Andersen, A. Mookerjee. Singapore, World Scientific.*

## NMTO

Andersen O. K., Saha-Dasupta, T.

Phys. Rev. B 62, R16219 (2000)



## What is “exact” in the EMTO method?

PRB Referee report (2004):

*“...The use of the term “exact” in connection with the EMTO label I find inappropriate and unfortunate, although I recognize that by this time it is written in stone. No significant aspect of any modern band structure method is exact...”*

The Schrödinger equation is solved “exactly” for the MT potential

- “exact” kinetic energy
- “exact” charge density



# Density Functional Theory

*Consider a system of  $N$  interacting electrons. The total energy is:*

$$E_e = T + E_{ee} + E_{en} + E_{nn}$$

*Total energy is a functional of the electron density  $n(\mathbf{r})$*

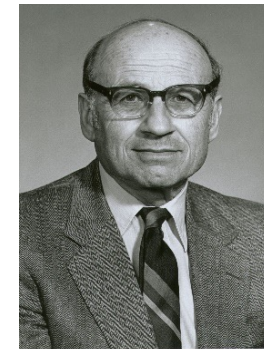
$$E_e = E[n]$$

where  $\int n(\mathbf{r})d\mathbf{r} = N$

all trial densities should contain the same number of electrons



P.C. Hohenberg



W. Kohn

1964

# Minimizing the total energy functional

- *We should plug in all possible  $n(r)$  in  $E[n]$*
- *$n(r)$  should be consistent with the number of electrons*
- *search until we find the minimum of  $E[n]$*

$$\min_n E[n] = E_0$$

*$\Rightarrow$  Schrödinger equation is solved!*

*In practice this route based on variational principle is not feasible because we do not know the exact form of  $E[n]$*

***DFT-level approximations are needed!***

# Restructuring the total energy functional

We separate the known parts of  $E[n]$

$$E[n] = T_s[n] + \frac{1}{2} \int v_H([n]; r) n(r) dr + \int v_e([n]; r) n(r) dr + E_{xc}[n]$$

known terms (large terms)

$T_s[n]$       **kinetic energy of non-interacting electrons**

$v_H([n]; r) = 2 \int \frac{n(r')}{|r - r'|} dr'$       **Hartree potential**

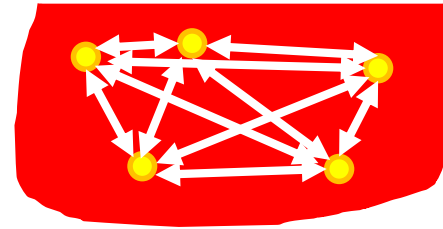
$v_e(r) = - \sum_R \frac{2Z_R}{|r - R|}$       **external potential**

and the rest (small terms)

$E_{xc}[n]$       **exchange-correlation energy**

# From the original interacting system to the non-interacting model system

*Interacting electrons in external potential:  
(original many-body problem)*



$V_e([n]; r)$

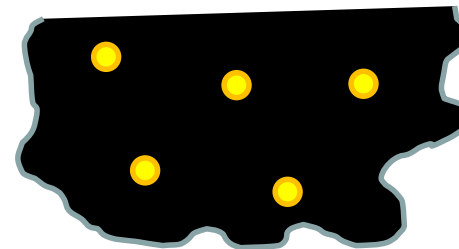
$$E[n] = T_s[n] + \frac{1}{2} \int v_H([n]; r) n(r) dr + \int v_e([n]; r) n(r) dr + E_{xc}[n]$$

Non-interacting electrons moving in an effective potential:

Note: the potential involves the **functional derivative** of the xc energy

$$E[n] = T_s[n] + \int v([n]; r) n(r) dr$$

$$v([n]; r) = v_e(r) + v_H([n]; r) + \frac{\delta E_{xc}[n]}{\delta n(r)}$$



$V([n]; r)$

# Kohn-Sham equations

*We can solve the non-interacting system which by construction leads to the same density as the real system*

$$\{-\nabla^2 + v([n]; \mathbf{r})\} \Psi_j(\mathbf{r}) = \varepsilon_j \Psi_j(\mathbf{r})$$

In KS scheme, the wave function depends only on the position of one single electron

**Self consistent solution:**

**input = output**

**Effective potential:**

$$v([n]; \mathbf{r}) = v_e(\mathbf{r}) + v_H([n]; \mathbf{r}) + \frac{\delta E_{xc}[n]}{\delta n(\mathbf{r})}$$

$$n(\mathbf{r}) = \sum_{\varepsilon_j \leq \varepsilon_F} |\Psi_j(\mathbf{r})|^2$$

Compare with Schrödinger eq.

$$\hat{H}\Psi_k = E_k \Psi_k$$
$$\Psi_k(\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N)$$

# Solving the Kohn-Sham single-electron equations

$$\left( -\frac{\nabla^2}{2} + V_{\text{eff}}(\mathbf{r}) \right) \psi_p(\mathbf{r}) = \varepsilon_p \psi_p(\mathbf{r})$$

Two methods to get Kohn-Sham orbitals:

1. Solve Kohn-Sham equation *directly* on a real-space grid (grid methods).
2. Use some basis functions for representation of Kohn-Sham orbitals:

$$\psi_p(\mathbf{r}) = \sum_i C_{pi} \varphi_i; \quad \varphi_i \text{ are basis functions}$$

The choice of the basis functions in principle does not matter for the final result, however, if it is done in a clever way, it makes calculations efficient.

The great variety of first-principles methods is about this point: optimization of the basis. Our computers are not powerful enough even to solve accurately Kohn-Sham equations without using special numerical tricks.

# Variational principle for the Kohn-Sham equation

$$\delta \left[ \langle \psi | H | \psi \rangle - E (\langle \psi | \psi \rangle - N) \right] / \delta \psi = 0$$

$$\psi = \sum_i c_i \varphi_i \quad \langle \psi | H | \psi \rangle = \sum_{ij} c_i^* c_j H_{ij} \quad \text{where } H_{ij} = \int d\mathbf{r} \varphi_i^*(\mathbf{r}) H \varphi_j(\mathbf{r})$$

In general (if the basis functions are not orthonormal):

$$\langle \psi | \psi \rangle = \sum_{ij} c_i^* c_j S_{ij} \quad \text{where } S_{ij} = \int d\mathbf{r} \varphi_i^*(\mathbf{r}) \varphi_j(\mathbf{r}) \quad \text{it is called overlap matrix}$$

Here,  $c_i$  are the coefficients to be found. 
$$\delta \left[ \sum_{ij} c_i^* c_j H_{ij} - \epsilon \sum_{ij} c_i^* c_j S_{ij} \right] / \delta c_i^* = 0$$

$$\sum_j c_j (H_{ij} - \epsilon S_{ij}) = 0 \quad \text{This is a homogeneous set of linear equations for } c \text{ and } \epsilon$$

It has non-trivial (not 0) solutions only if the determinant vanishes:  
This equation gives the one electron energies ( $\epsilon$ )

$$\det[\mathbf{H} - \epsilon \mathbf{S}] = 0$$

# **The EMTO method, Implementation (1998-2001)**

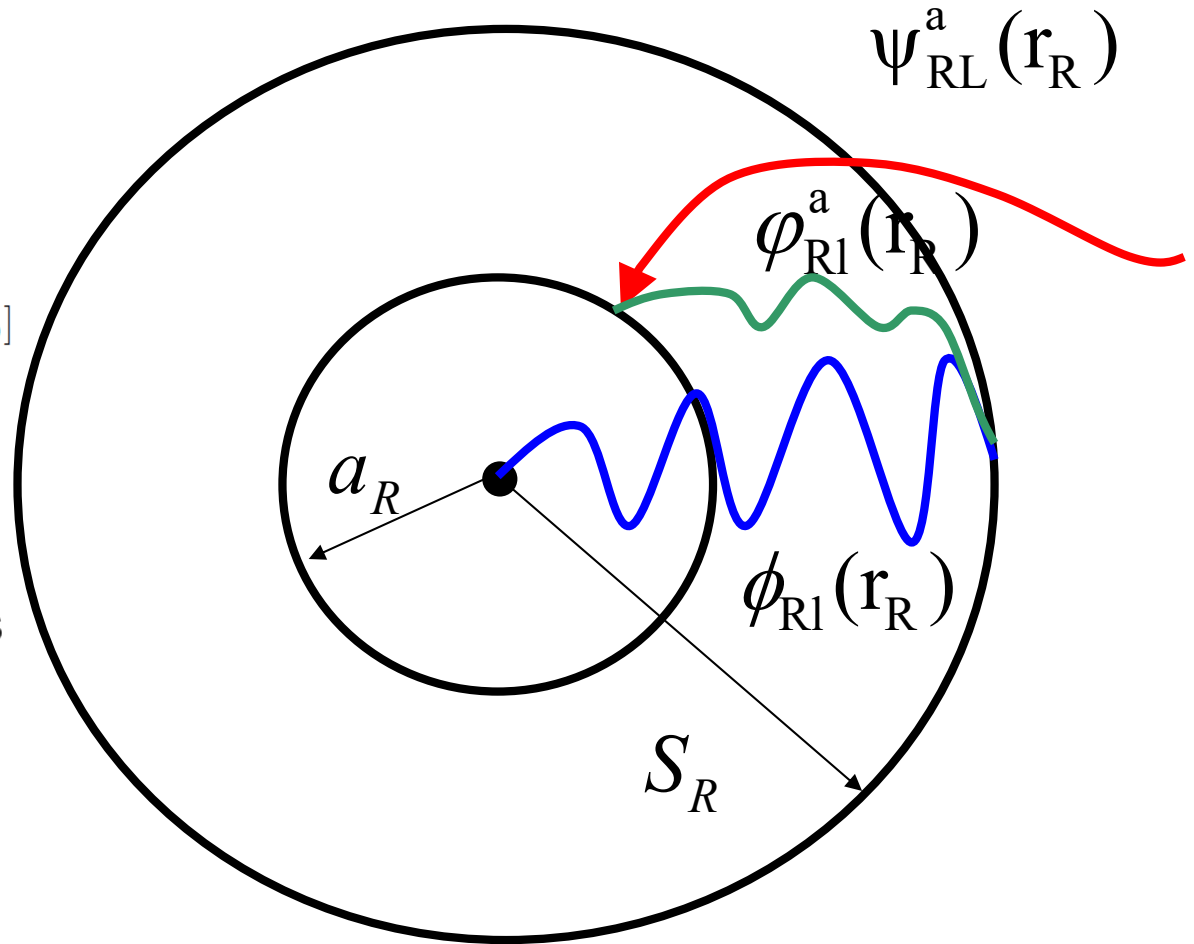


# The EMTO formalism

The KS potential is approximated by the overlapping optimized muffin-tin potential

$$v(\mathbf{r}) \approx v_{mt}(\mathbf{r}) \equiv v_0 + \sum_R [v_R(r_R) - v_0]$$

$v_R(r_R)$  is spherical for  $r_R \leq S_R$  and  $v_R(r_R) = v_0$  for  $r_R > S_R$   
 $v_0$  is the constant potential connecting the local potential wells



$$\Psi_{RL}^a(\mathbf{r}_R)$$

**Screened spherical wave (constant potential)**

$$\phi_{Rl}^a(\mathbf{r}_R)$$

**Local free electron solution (constant potential)**

$$\phi_{Rl}(\mathbf{r}_R)$$

**Partial wave (solution of the spherical Schrödinger eq.)**

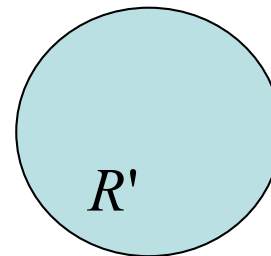
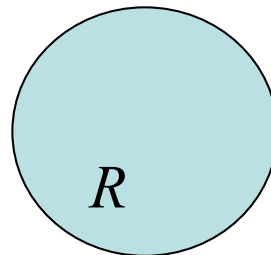
# The screened spherical waves; $S_{R'L'RL}^a$

Solutions for the constant potential (Bessel and Neumann functions):

$$\left\{ \nabla^2 + \kappa^2 \right\} \psi_{RL}^a(\kappa^2, \mathbf{r}_R) = 0, \quad \kappa^2 \equiv \epsilon - v_0.$$

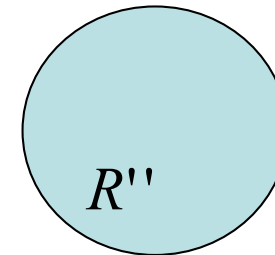
Screening is realized with "hard" spheres of radius  $a_R$ :

$$\psi_{RL}^a(a_R) \propto Y_L(\hat{\mathbf{r}}_R)$$



$$\psi_{RL}^a(a_{R'}) = 0$$

$$\psi_{RL}^a(a_{R''}) = 0$$



Boundary conditions require a multi-center form:

$$\begin{aligned} \psi_{RL}^a(\kappa^2, \mathbf{r}_R) &= f_{RL}^a(\kappa^2, r_R) Y_L(\hat{\mathbf{r}}_R) \delta_{RR'} \delta_{LL'} \\ &+ \sum_{L'} g_{R'L'}^a(\kappa^2, r_{R'}) Y_{L'}(\hat{\mathbf{r}}_{R'}) S_{R'L'RL}^a(\kappa^2). \end{aligned}$$

# The screened spherical waves

$$\begin{aligned} \psi_{RL}^a(\kappa^2, \mathbf{r}_R) &= f_{Rl}^a(\kappa^2, r_R) Y_L(\hat{r}_R) \delta_{RR'} \delta_{LL'} \\ &+ \sum_{L'} g_{R'l'}^a(\kappa^2, r_{R'}) Y_{L'}(\hat{r}_{R'}) S_{R'l'RL}^a(\kappa^2). \end{aligned}$$

$$f_{Rl}^a(\kappa^2, r)|_{a_R} = 1 \quad \text{and} \quad g_{Rl}^a(\kappa^2, r)|_{a_R} = 0.$$

$$\left. \frac{\partial f_{Rl}^a(\kappa^2, r)}{\partial r} \right|_{a_R} = 0 \quad \text{and} \quad \left. \frac{\partial g_{Rl}^a(\kappa^2, r)}{\partial r} \right|_{a_R} = \frac{1}{a_R}.$$

**Linear combinations of the Bessel and Neumann functions:**

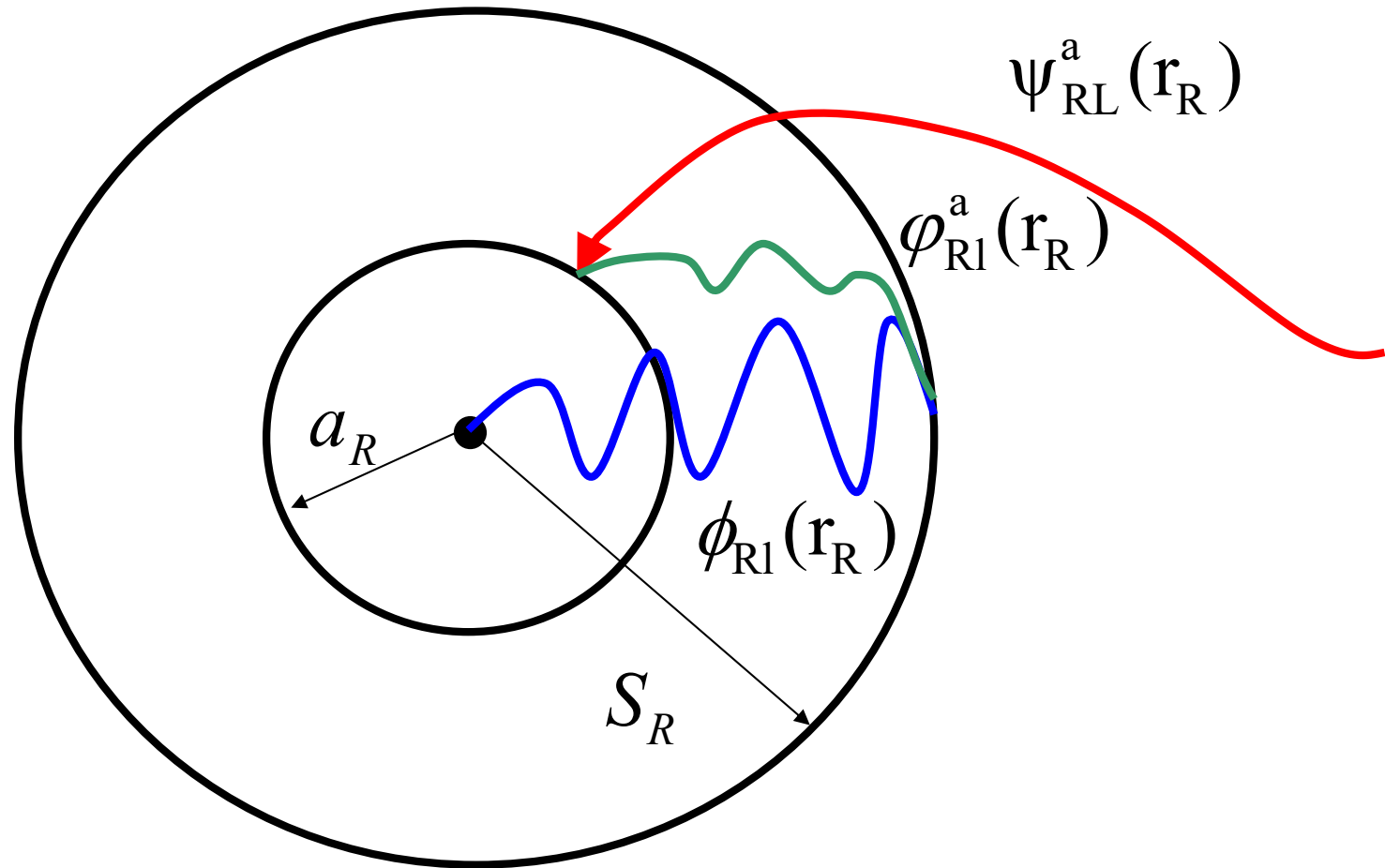
$$f_{Rl}^a(\kappa^2, r) = t_{Rl}^1(\kappa^2) n_l(\kappa^2, r) + t_{Rl}^2(\kappa^2) j_l(\kappa^2, r)$$

$$g_{Rl}^a(\kappa^2, r) = -t_{Rl}^3(\kappa^2) n_l(\kappa^2, r) - t_{Rl}^4(\kappa^2) j_l(\kappa^2, r).$$

**Screening matrix:**

$$\begin{Bmatrix} t_{Rl}^1(\kappa^2) & t_{Rl}^2(\kappa^2) \\ t_{Rl}^3(\kappa^2) & t_{Rl}^4(\kappa^2) \end{Bmatrix} = 2 \frac{a_R^2}{w} \begin{Bmatrix} \frac{\partial j_l(\kappa^2, a_R)}{\partial r_R} & -\frac{\partial n_l(\kappa^2, a_R)}{\partial r_R} \\ \frac{1}{a_R} j_l(\kappa^2, a_R) & -\frac{1}{a_R} n_l(\kappa^2, a_R) \end{Bmatrix}.$$

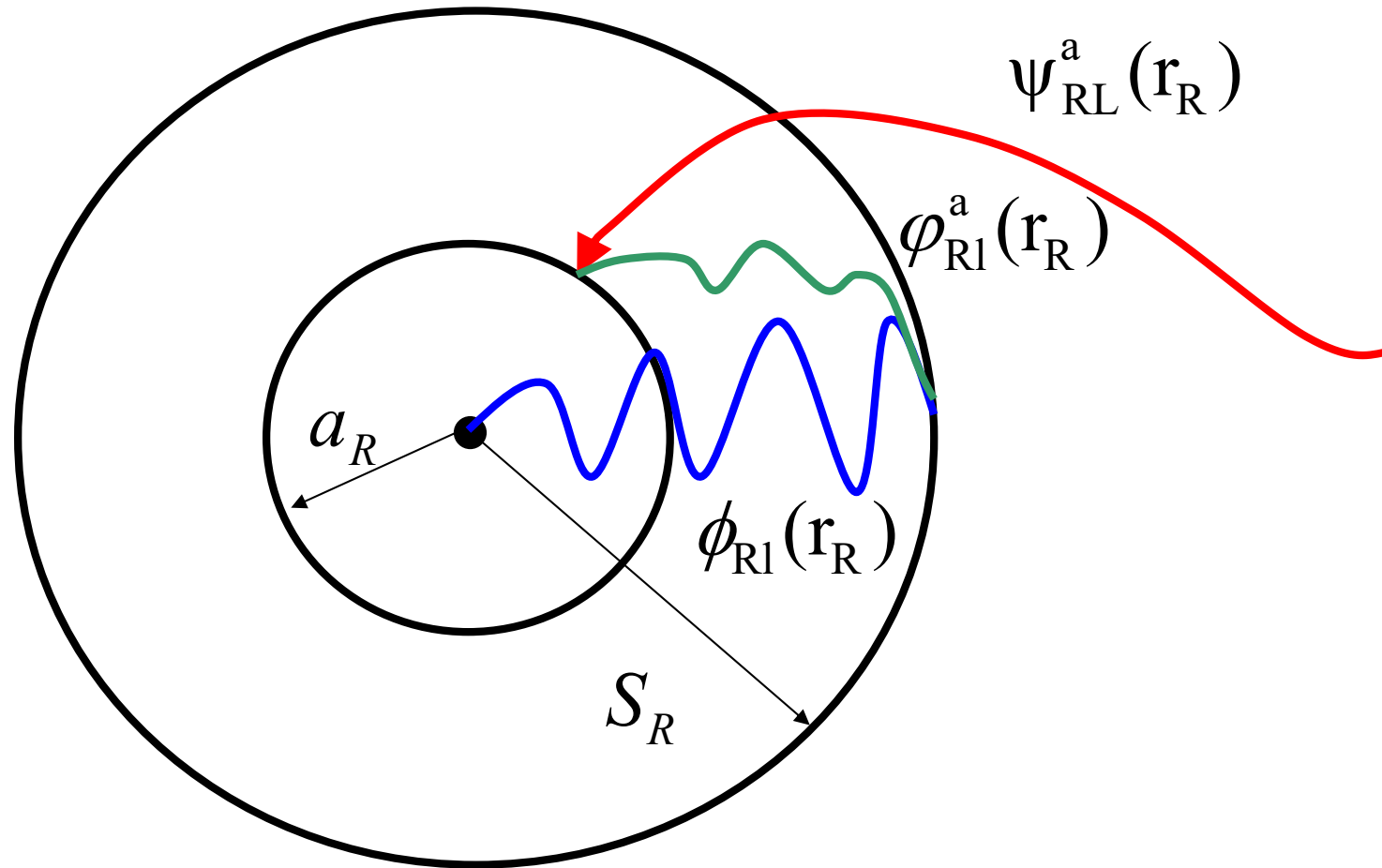
# The local free electron solution



$$\phi_{Rl}^a(\epsilon, r_R) = f_{Rl}^a(\kappa^2, r_R) + g_{Rl}^a(\kappa^2, r_R) D_{Rl}^a(\epsilon),$$

**By construction, it joins the screened spherical wave at  $a_R$   
There is a slope difference (first order derivative is discontinuous).**

# Partial wave; $D_{Rl}^a$



It is the solution of the radial Schrodinger equation for  $r_R \leq S_R$ , potential  $v_R(r_R)$ .  
It joins continuously the local free electron solution at  $S_R$ .  
This condition gives the slope of the local free electron solution at  $a_R$  ( $D_{Rl}^a$ ).

# The kink cancellation condition

The Exact Muffin-Tin Orbitals:

$$\begin{aligned}
 \bar{\psi}_{RL}^a(\epsilon, \mathbf{r}_R) &= \psi_{RL}^a(\kappa^2, \mathbf{r}_R) + N_{Rl}^a(\epsilon) \phi_{Rl}(\epsilon, r_R) Y_L(\hat{r}_R) \\
 &\quad - \varphi_{Rl}^a(\epsilon, r_R) Y_L(\hat{r}_R), \\
 \Psi(\mathbf{r}_R) &= \sum_L N_{Rl}^a(\epsilon) \phi_{Rl}(\epsilon, r_R) Y_L(\hat{r}_R) v_{RL}^a \\
 &\quad + \sum_L \left[ f_{Rl}^a(\kappa^2, r_R) v_{RL}^a + g_{Rl}^a(\kappa^2, r_R) \sum_{R'L'} S_{RLR'L'}^a(\kappa^2) v_{R'L'}^a \right] Y_L(\hat{r}_R) \\
 &\quad - \sum_L [f_{Rl}^a(\kappa^2, r_R) + g_{Rl}^a(\kappa^2, r_R) D_{Rl}^a(\epsilon)] Y_L(\hat{r}_R) v_{RL}^a. \tag{2.29}
 \end{aligned}$$

It is solution for the full Schrödinger equation if the second and third terms vanish:

$$\sum_{RL} a_{R'} \left[ S_{R'L'RL}^a(\kappa_j^2) - \delta_{R'R} \delta_{L'L} D_{Rl}^a(\epsilon_j) \right] v_{RL,j}^a = 0,$$

Overlap matrix :

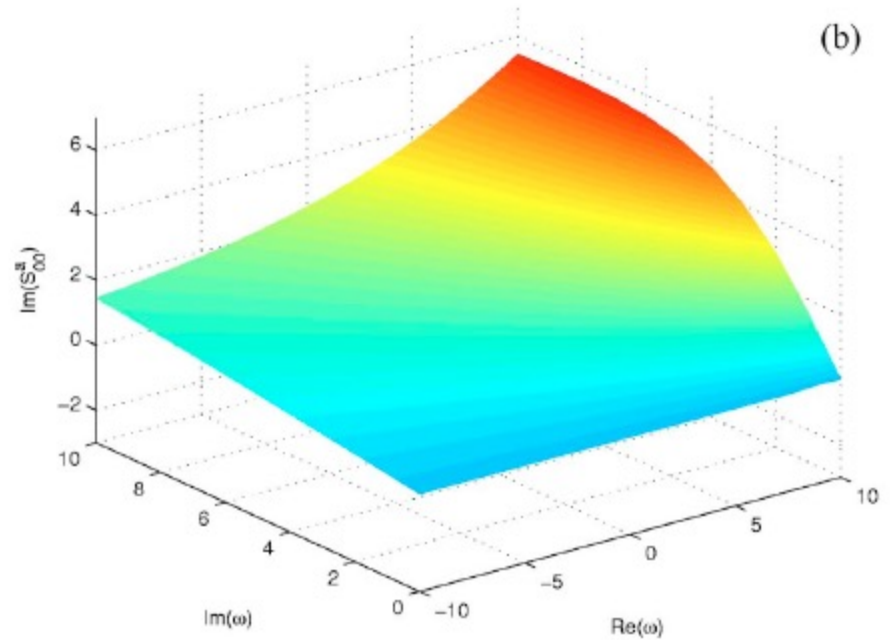
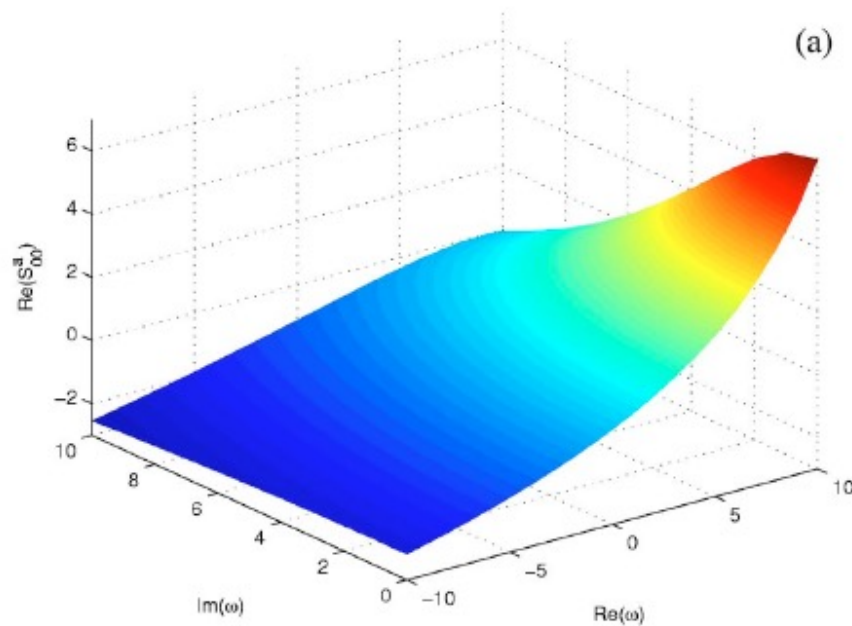
$$\begin{aligned}
 &\int \bar{\psi}_{R'L'}^*(\epsilon, \mathbf{r}) \bar{\psi}_{RL}(\epsilon, \mathbf{r}) d\mathbf{r} \\
 &= a_R \dot{S}_{R'L'RL}^a(\kappa^2) - a_R \dot{D}_{Rl}^a(\epsilon) = \dot{K}_{R'L'RL}^a(\epsilon).
 \end{aligned}$$

# Slope matrix

$$\kappa^2 \equiv \epsilon - v_0,$$

$$S_{R'L'RL}^a = \frac{t_{RL}^1}{t_{RL}^3} \delta_{R'R} \delta_{L'L} + \frac{1}{t_{R'L'}^3} \left[ -S^0 - \frac{t_{RL}^4}{t_{RL}^3} \right]_{R'L'RL}^{-1} \frac{d_{RL}^a}{t_{RL}^3},$$

$$n_L(\kappa^2, \mathbf{r}_R) = - \sum_{L'} j_{L'}(\kappa^2, \mathbf{r}_{R'}) S_{R'L'RL}^0(\kappa^2).$$



# The effect of the hard (screening) sphere radius

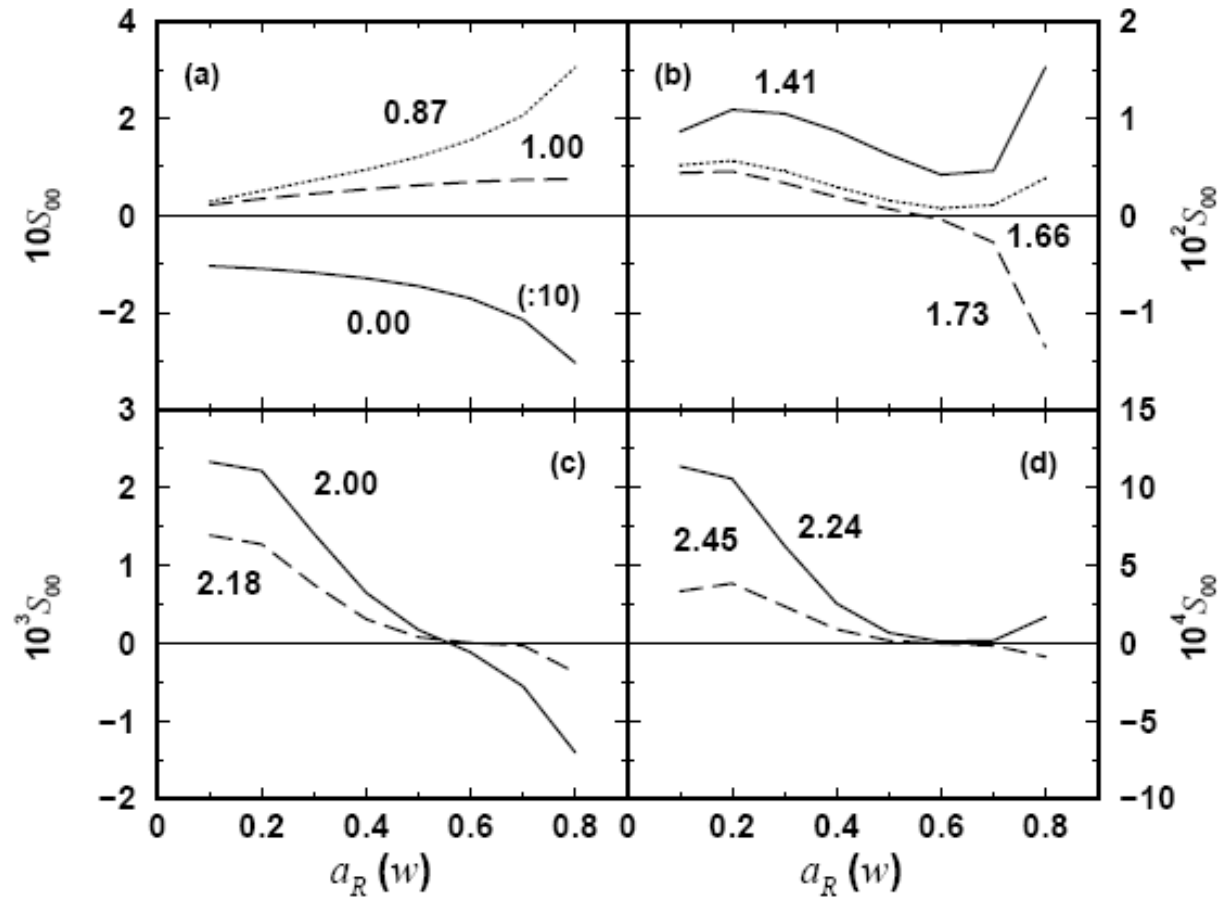


Fig. 3.1. The  $ss$  element of the  $bcc$  slope matrix for  $\omega = 0$  plotted as a function of the hard sphere radius  $a_R$  and the radius of the coordination shell  $d_{R'R}$  (shown by numbers in units of lattice constant). Note that in panel (a), the scale for  $d_{R'R} = 0.00a$  has been divided by 10.

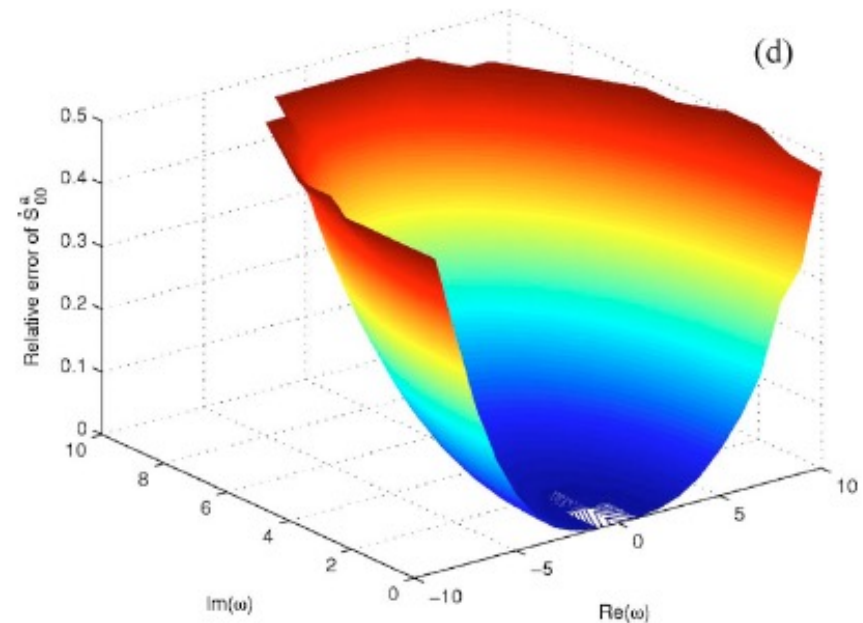
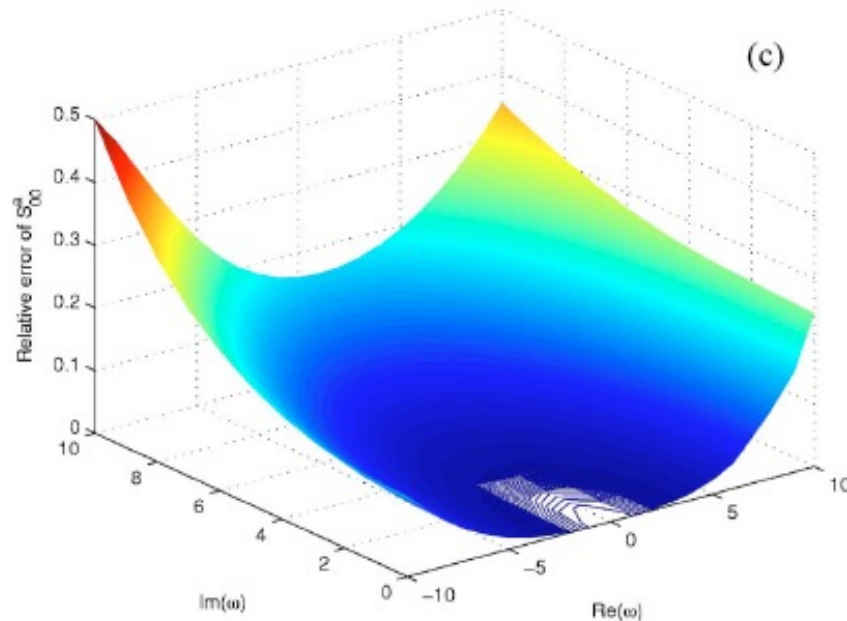


# Parametrization of the slope matrix

$$S^a(\omega) \approx S_n^a(\omega; \omega_0) \equiv S^a(\omega_0) + \frac{1}{1!} \frac{dS^a(\omega)}{d\omega} (\omega - \omega_0) + \frac{1}{2!} \frac{d^2 S^a(\omega)}{d\omega^2} (\omega - \omega_0)^2 + \dots + \frac{1}{n!} \frac{d^n S^a(\omega)}{d\omega^n} (\omega - \omega_0)^n.$$

$\kappa^2 \equiv \epsilon - v_0,$   
 $\omega \equiv (\kappa W)^2$

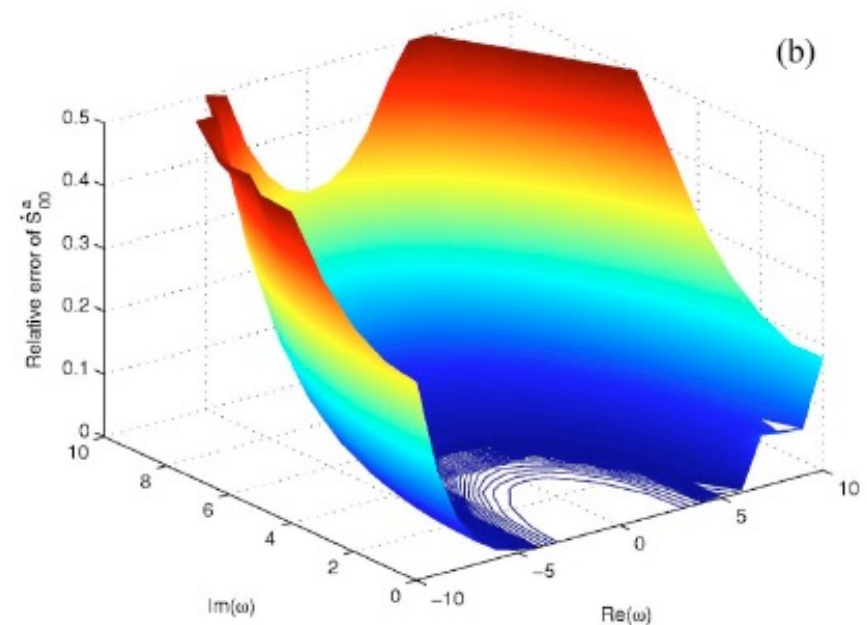
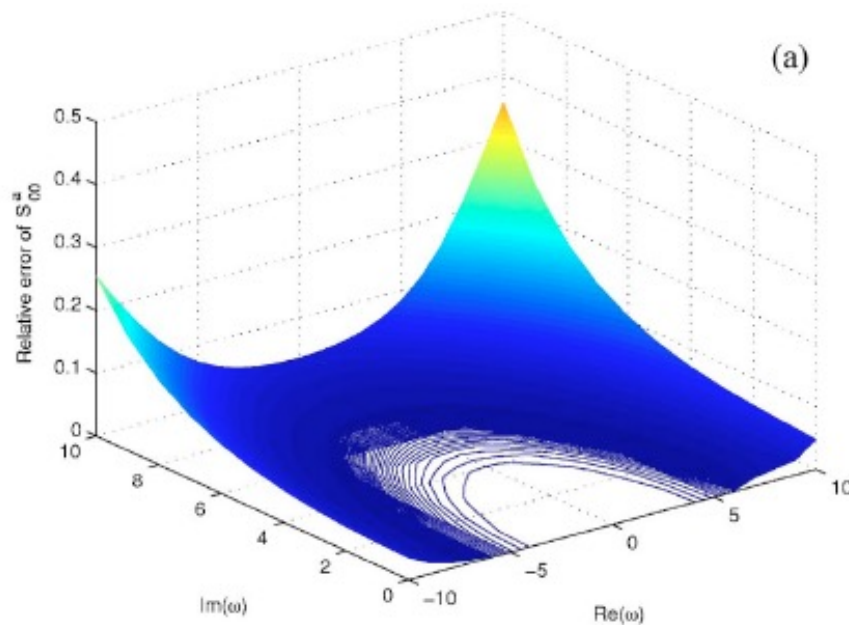
Slope matrix and first derivative (3<sup>rd</sup> order single-center expansion)



# Parametrization of the slope matrix

$$S^a(\omega) \approx S_n^a(\omega; \omega_0) \equiv S^a(\omega_0) + \frac{1}{1!} \frac{dS^a(\omega)}{d\omega} (\omega - \omega_0) + \frac{1}{2!} \frac{d^2 S^a(\omega)}{d\omega^2} (\omega - \omega_0)^2 + \cdots + \frac{1}{n!} \frac{d^n S^a(\omega)}{d\omega^n} (\omega - \omega_0)^n. \quad \omega \equiv (\kappa W)^2$$

Slope matrix and first derivative (6<sup>th</sup> order single-center expansion)

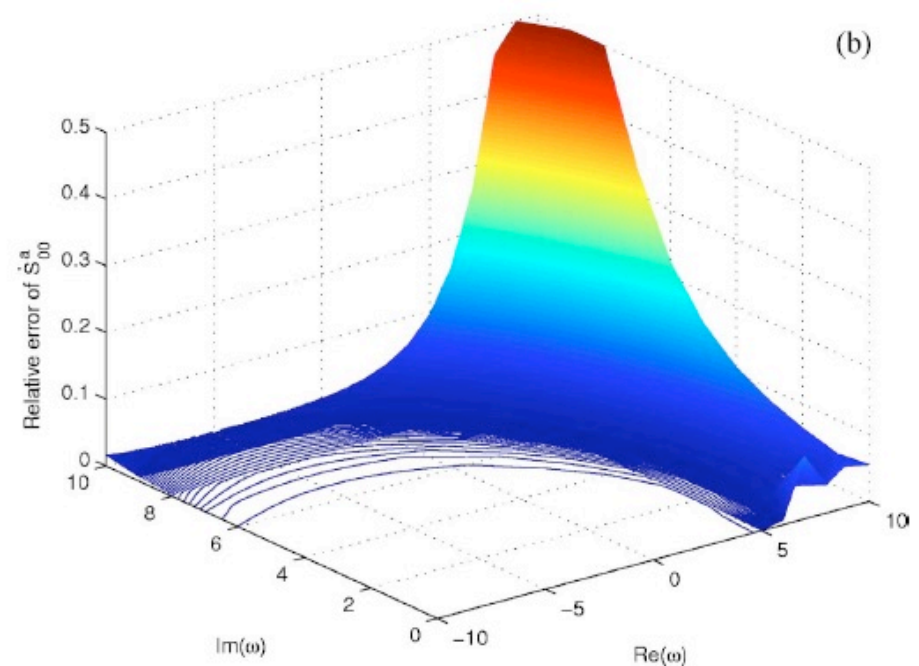
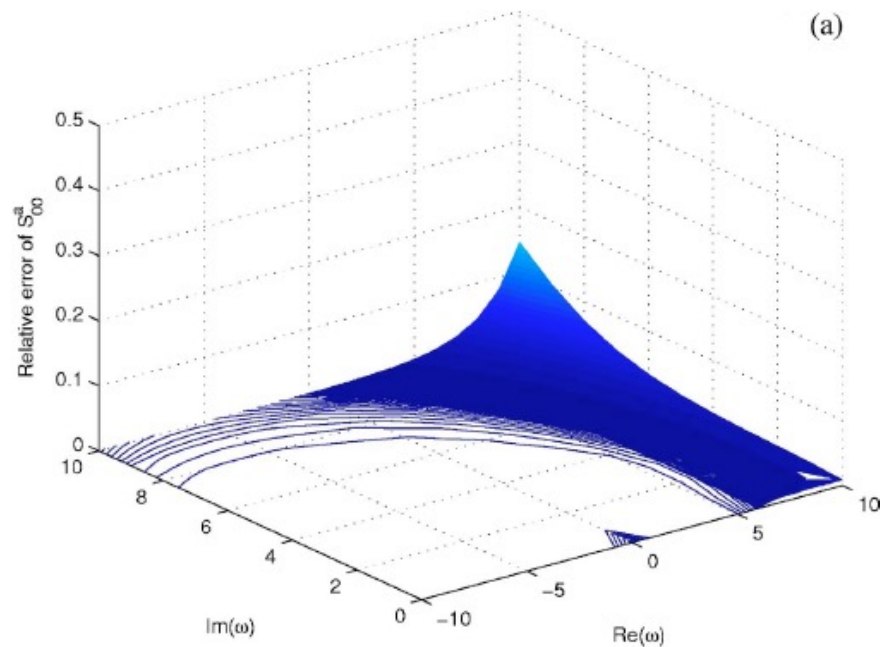


# Parametrization of the slope matrix

$$\begin{aligned}
 S^a(\omega) &\approx S_{n,m}^a(\omega; \omega_1, \omega_2) = S_n^a(\omega; \omega_1) \\
 &+ \frac{1}{(n+1)!} a_{n+1} (\omega - \omega_1)^{n+1} + \dots \\
 &+ \frac{1}{(n+m)!} a_{n+m+1} (\omega - \omega_1)^{n+m+1},
 \end{aligned}$$

$$\begin{aligned}
 S_{n,m}^a(\omega_2; \omega_1, \omega_2) &= S^a(\omega_2), \\
 \left. \frac{dS_{n,m}^a(\omega; \omega_1, \omega_2)}{d\omega} \right|_{\omega=\omega_2} &= \left. \frac{dS^a(\omega)}{d\omega} \right|_{\omega=\omega_2}, \dots \\
 \left. \frac{d^m S_{n,m}^a(\omega; \omega_1, \omega_2)}{d\omega^m} \right|_{\omega=\omega_2} &= \left. \frac{d^m S^a(\omega)}{d\omega^m} \right|_{\omega=\omega_2}.
 \end{aligned}$$

Slope matrix and first derivative (6+6<sup>th</sup> order two-center expansion)



# Accuracy: slope matrix and charge density

$$\Delta_e(l_{max}^h) = \sum_R \int_{\Omega_R} n(\mathbf{r}_R) d\mathbf{r}_R - N_e$$

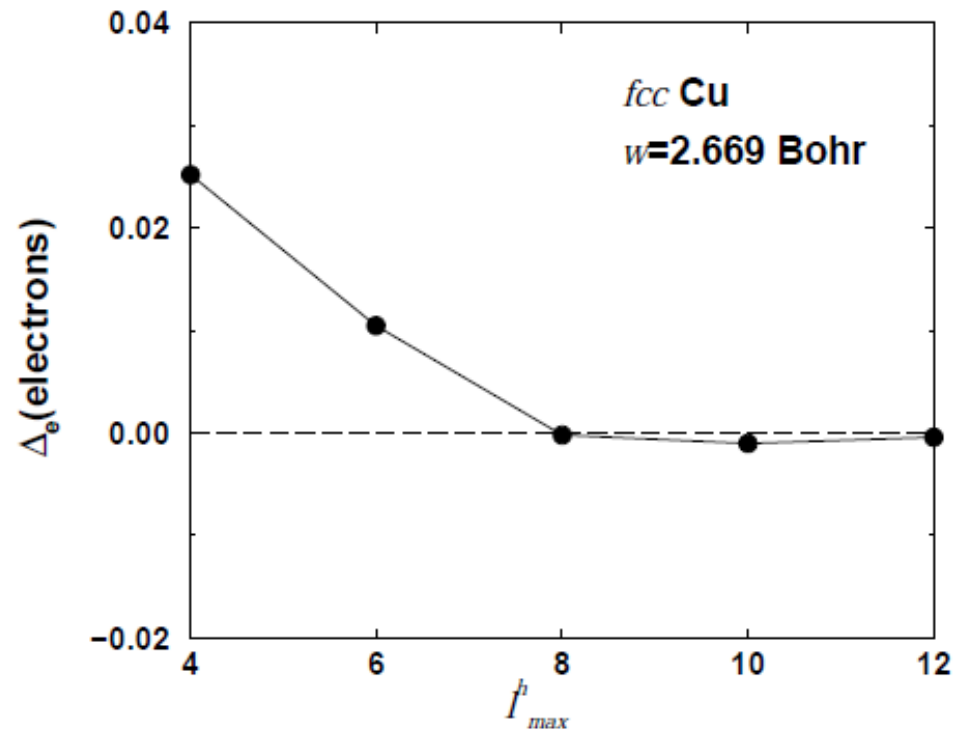


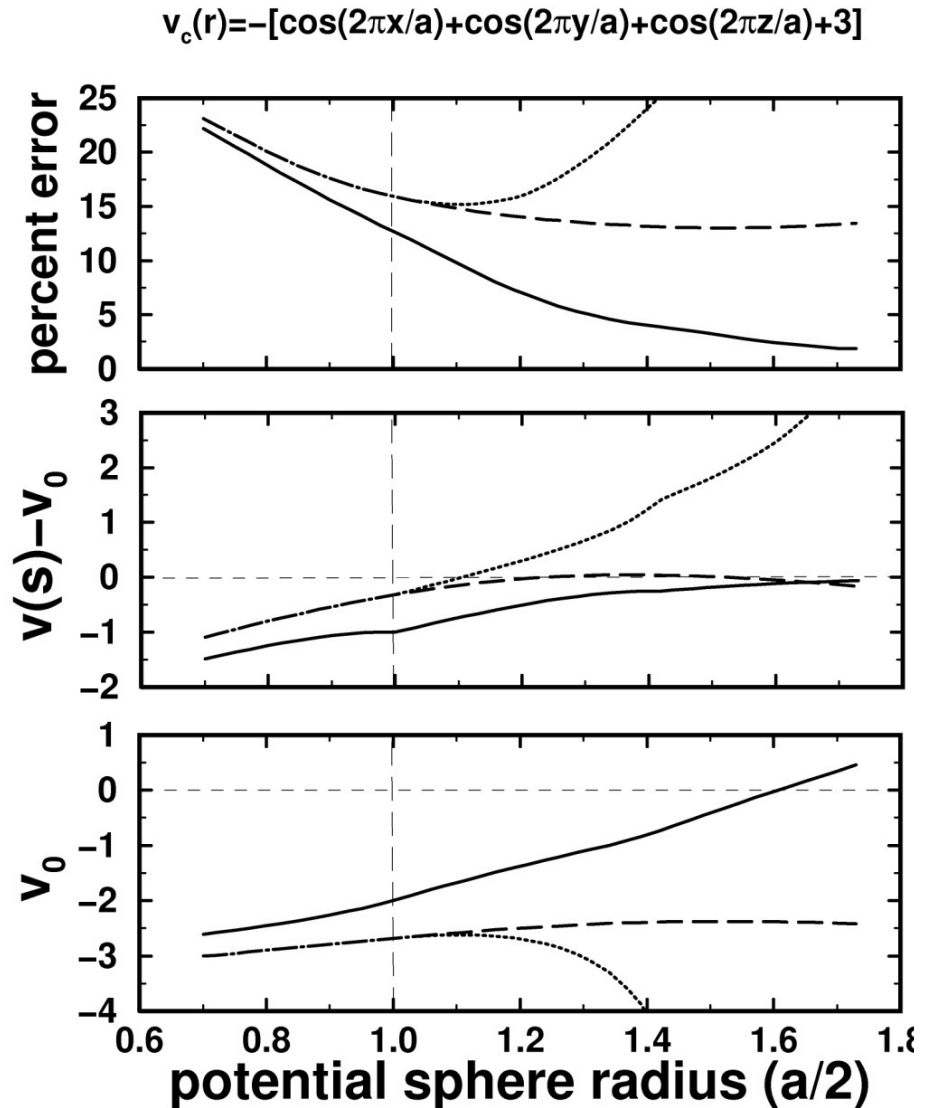
Fig. 4.7. The calculated charge misfit  $\Delta_e$  for *fcc* Cu plotted as a function of  $l_{max}^h$ .

# Optimized Overlapping Muffin-Tin potential

O. K. Andersen, et al. (1994)

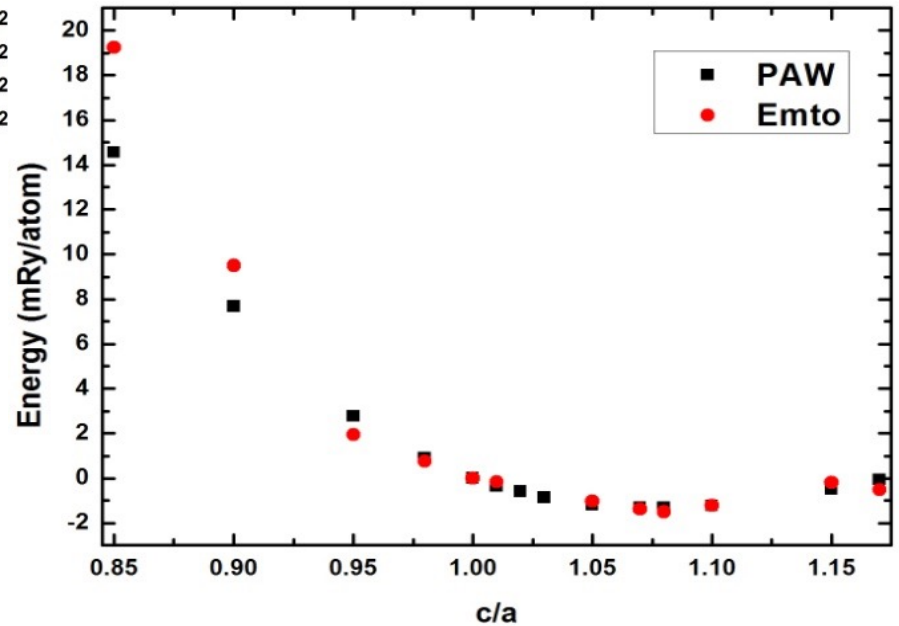
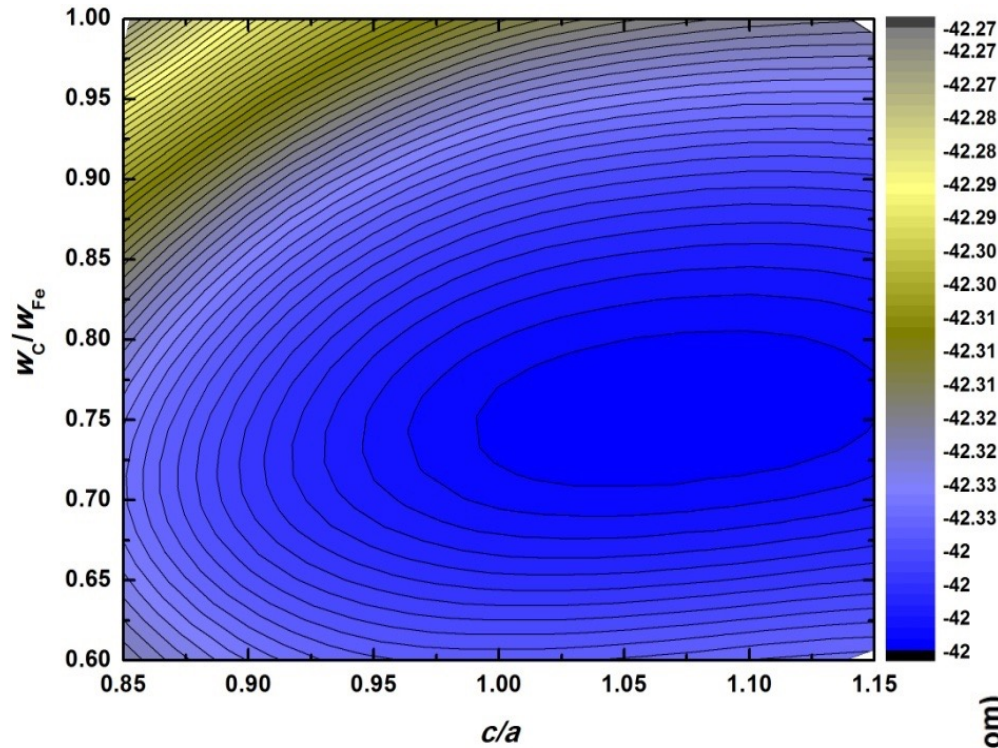
$$V_{\text{FP}}(\mathbf{r}) \approx V_{\text{mt}}(\mathbf{r})$$

$$V_{\text{mt}}(\mathbf{r}) = V_0 + \sum_{\mathbf{R}} [V_{\mathbf{R}}(r_{\mathbf{R}}) - V_0]$$



# Optimized Overlapping Muffin-Tin potential

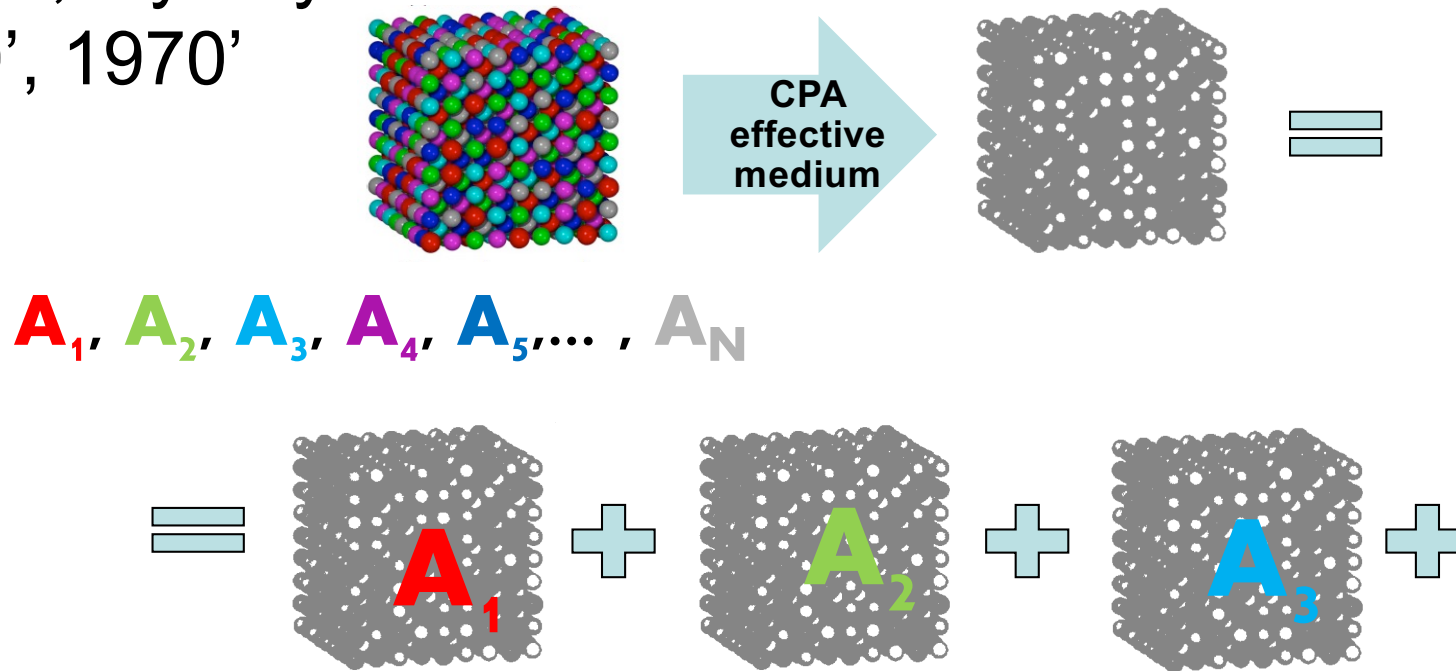
## Examples: Fe-C





# Coherent Potential Approximation

Soven, Györfy  
1960', 1970'



We solve N single impurity problems  
(order-N in terms of alloy components)

# The EMT0-CPA method for alloys

Kink cancelation for the effective medium

$$\sum_{Q''L''} a_{Q'} \left[ S_{Q'L'Q''L''}(\kappa^2, \mathbf{k}) - \delta_{Q'Q''} \tilde{D}_{Q'L'Q''L''}(z) \right] \times \tilde{g}_{Q''L''QL}(z, \mathbf{k}) = \delta_{Q'Q} \delta_{L'L},$$

Effective medium Green's function

$$\tilde{g}_{QLQL'}(z) = \sum_i c_Q^i g_{QLQL'}^i(z),$$

Impurity Green's function (Dyson eq.)

$$g_{QLQL'}^i(z) = \tilde{g}_{QLQL'}(z) + \sum_{L''L'''} \tilde{g}_{QLQL''}(z) \times \left[ D_{QL''}^i(z) \delta_{L''L'''} - \tilde{D}_{QL''QL'''}(z) \right] g_{QL''QL'}^i(z),$$

Self-consistent solution is needed.

Similar like in EMT0 but now it includes the impurity potentials and Green's functions.



# Total energy in EMTO/EMTO-CPA (The Full Charge Density method)

After we solve the KS equation

$$\{-\nabla^2 + v([\mathbf{n}]; \mathbf{r})\} \Psi_j(\mathbf{r}) = \varepsilon_j \Psi_j(\mathbf{r})$$

we construct the total charge density

$$n(\mathbf{r}) = \sum_{\varepsilon_j \leq \varepsilon_F} |\Psi_j(\mathbf{r})|^2$$

and then compute the total energy (valid both for ordered and disordered systems):

$$E[\mathbf{n}] = T_s[\mathbf{n}] + \frac{1}{2} \int v_H([\mathbf{n}]; \mathbf{r}) n(\mathbf{r}) d\mathbf{r} + \int v_e([\mathbf{n}]; \mathbf{r}) n(\mathbf{r}) d\mathbf{r} + E_{xc}[\mathbf{n}]$$

$c^i$  is the concentration for alloy component  $i$

$$E_{tot} = T_s[\mathbf{n}] + \sum_R \sum_i c^i (F_{intraR}^i[n_R^i] + E_{xcR}^i[n_R^i]) + F_{inter}[Q] + \Delta E^{SIM}.$$

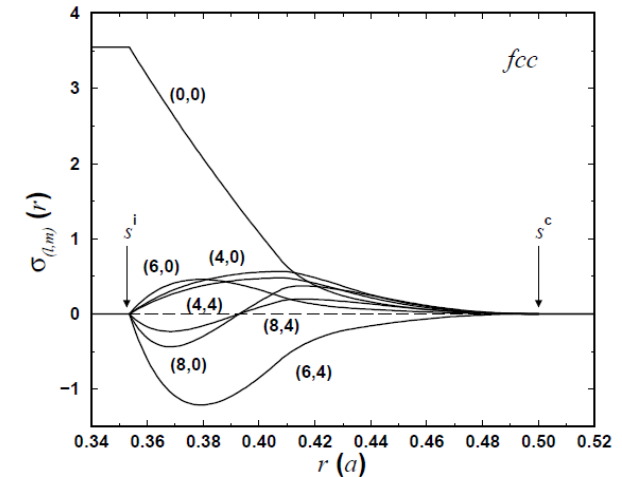
The last term is a “small” correction for random alloys (if CPA is involved).

## Annex: All integrations over the Wigner-Seitz cells are computed using the shape function technique

$$\sigma_R(\mathbf{r}_R) \equiv \begin{cases} 1 & \text{for } \mathbf{r}_R \in \Omega_R \\ 0 & \text{otherwise} \end{cases}.$$

$$\sigma_R(\mathbf{r}_R) = \sum_L \sigma_{RL}(r_R) Y_L(\hat{r}_R).$$

$$\int_{\Omega_R} n_R(\mathbf{r}_R) K([n]; \mathbf{r}_R) d\mathbf{r}_R = \int_{s_R^c} \sigma_R(\mathbf{r}_R) n_R(\mathbf{r}_R) K([n]; \mathbf{r}_R) d\mathbf{r}_R.$$



$\Omega$  is the WS cell,  
 $s^c$  is the circumscribed sphere  
radius

$$\sigma_R(\mathbf{r}_R) n_R(\mathbf{r}_R) = \sum_L \tilde{n}_{RL}(r_R) Y_L(\hat{r}_R).$$

$$\int_{\Omega_R} n_R(\mathbf{r}_R) K([n]; \mathbf{r}_R) d\mathbf{r}_R = \sum_L \int_0^{s_R^c} \tilde{n}_{RL}(r_R) K_L(r_R) r_R^2 dr_R,$$

$$K_L(r_R) \equiv \int K([n]; \mathbf{r}_R) Y_L(\hat{r}_R) d\hat{r}_R$$

Most of the 3D integrals are reduced to 1D integrals.

# Total energy: kinetic energy

Kinetic energy is computed from the Kohn-Sham wave functions or one-electron energies minus a potential dependent term:

$$\begin{aligned} T_s[n] &\equiv \sum_{\epsilon_j \leq \epsilon_F} \int \Psi_j^*(\mathbf{r}) (-\nabla^2) \Psi_j(\mathbf{r}) d\mathbf{r} \\ &= \sum_{\epsilon_j \leq \epsilon_F} \epsilon_j - \int n(\mathbf{r}) v([\mathbf{n}]; \mathbf{r}) d\mathbf{r}. \end{aligned}$$

$$E[n] = T_s[n] + \frac{1}{2} \int v_H([\mathbf{n}]; \mathbf{r}) n(\mathbf{r}) d\mathbf{r} + \int v_e([\mathbf{n}]; \mathbf{r}) n(\mathbf{r}) d\mathbf{r} + E_{xc}[n]$$

The second equation comes from the Kohn-Sham equation.

**The first term is the one electron energy or band energy.**

# Total energy: intracell energy

Intracell energy is the Coulomb energy between electrons within the unit cell:

$$E[n] = T_s[n] + \frac{1}{2} \int v_H([n]; r) n(r) dr + \int v_e([n]; r) n(r) dr + E_{xc}[n]$$

$$F_{intraR}^i[n_R^i] = \frac{\sqrt{4\pi}}{w} \sum_L \int_0^{s_R^c} \tilde{n}_{RL}^i(r_R) \left[ \left( \frac{r_R}{w} \right)^l P_{RL}^i(r_R) + \left( \frac{r_R}{w} \right)^{-l-1} Q_{RL}^i(r_R) - 2Z_R^i \frac{w}{r_R} \delta_{L,L_0} \right] r_R^2 dr_R$$

$$P_{RL}^i(r_R) \equiv \frac{\sqrt{4\pi}}{2l+1} \int_{r_R}^{s_R^c} \tilde{n}_{RL}^i(r'_R) \left( \frac{r'_R}{w} \right)^{-l-1} (r'_R)^2 dr'_R,$$

$$Q_{RL}^i(r_R) \equiv \frac{\sqrt{4\pi}}{2l+1} \int_0^{r_R} \tilde{n}_{RL}^i(r'_R) \left( \frac{r'_R}{w} \right)^l (r'_R)^2 dr'_R.$$

# Total energy: intercell energy

Intercell (Madelung) energy is the Coulomb energy between electrons within different unit cell:

$$F_{inter}^{no}[n] = \frac{1}{2w} \sum_{RR'}' \sum_{LL'} Q_{RL} M_{RLR'L'} Q_{R'L'}.$$

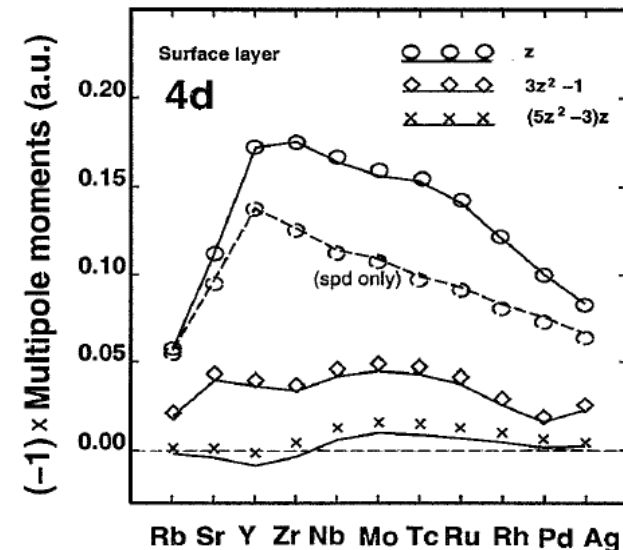
Multipole moment of the charge density:

$$Q_{RL}^i = \frac{\sqrt{4\pi}}{2l+1} \int_0^{s_R^c} \left(\frac{r_R}{w}\right)^l \tilde{n}_{RL}^i(r_R) r_R^2 dr_R - Z_R^i \delta_{L,L_0}.$$

$$Q_{RL} = \sum_i c_R^i Q_{RL}^i,$$

$$E[n] = T_s[n] + \frac{1}{2} \int v_H([n]; r) n(r) dr + \int v_e([n]; r) n(r) dr + E_{xc}[n]$$

$Q_{lm=0}$  moments for fcc (111) surface



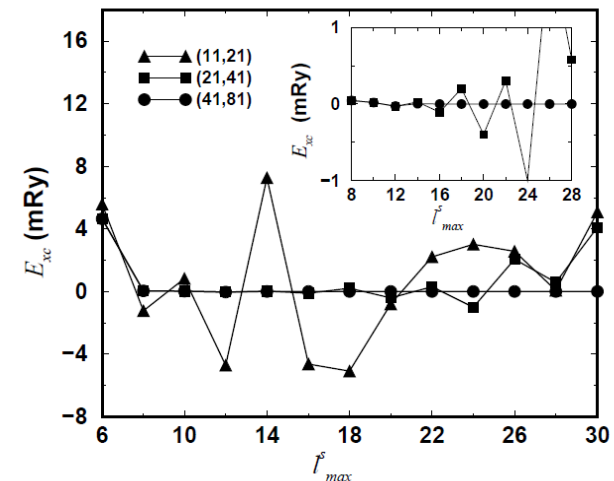
# Total energy: xc energy

Exchange and correlation energy from 3D integration:

$$E[n] = T_s[n] + \frac{1}{2} \int v_H([n]; r) n(r) dr + \int v_e([n]; r) n(r) dr + E_{xc}[n]$$

$$E_{xc}[n_R] = \int_0^{2\pi} \int_0^\pi \int_0^{s_R^c} n_R^i(\mathbf{r}_R) \varepsilon_{xc}([n_R^i]; \mathbf{r}_R) \times \sum_L^{l_{max}^s} \sigma_{RL}(r_R) Y_L(\hat{r}_R) r_R^2 dr_R \sin \theta d\theta d\phi$$

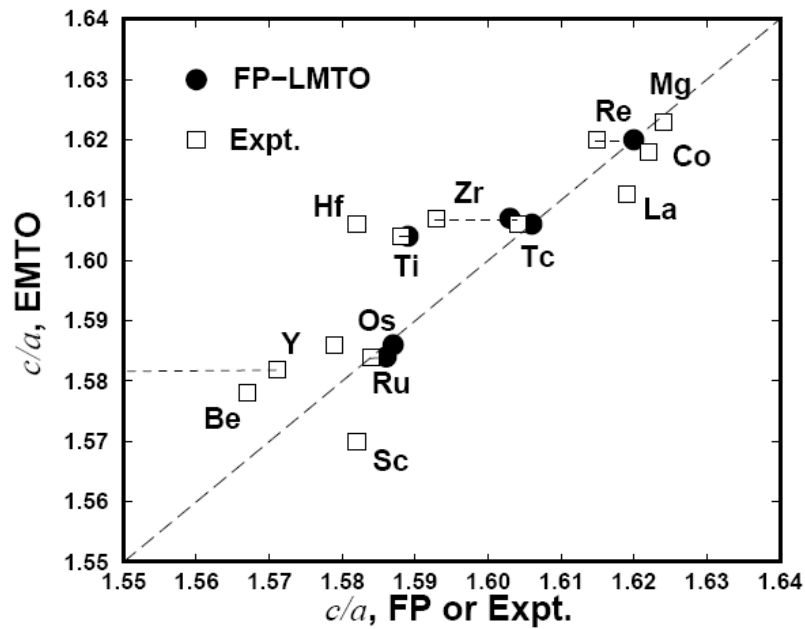
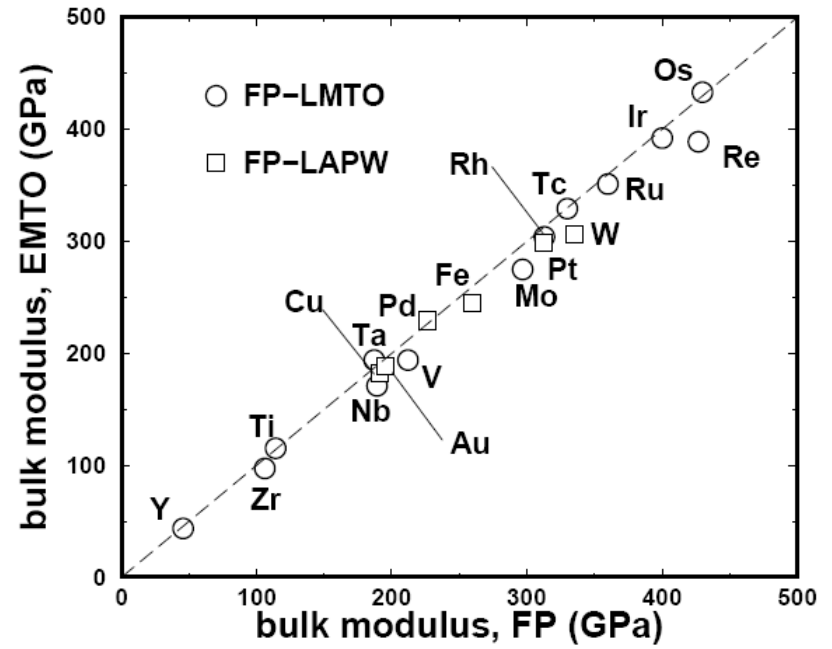
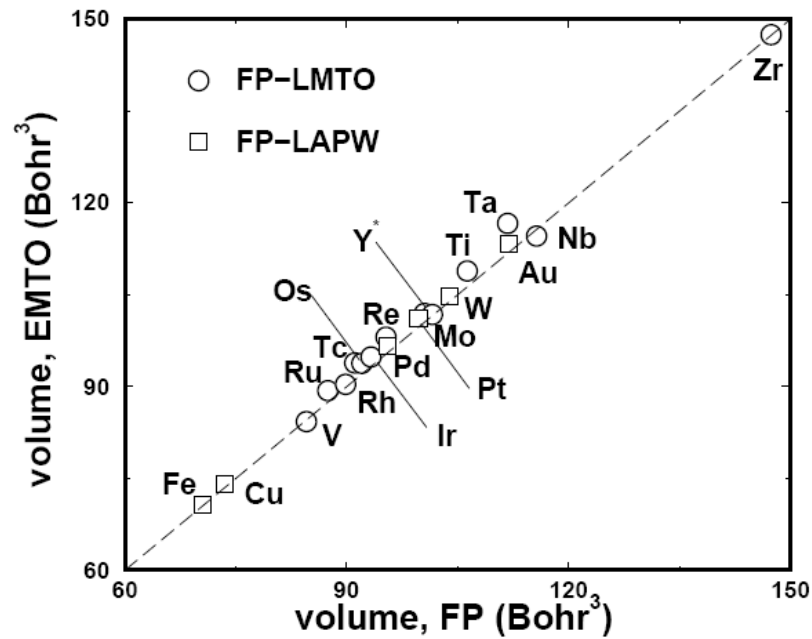
Very slow convergence with respect to the number of angular mesh points and  $l$ -truncation.



**Demonstration**

**Pioneering test  
calculations**

# Bulk properties





# Surface properties: stress

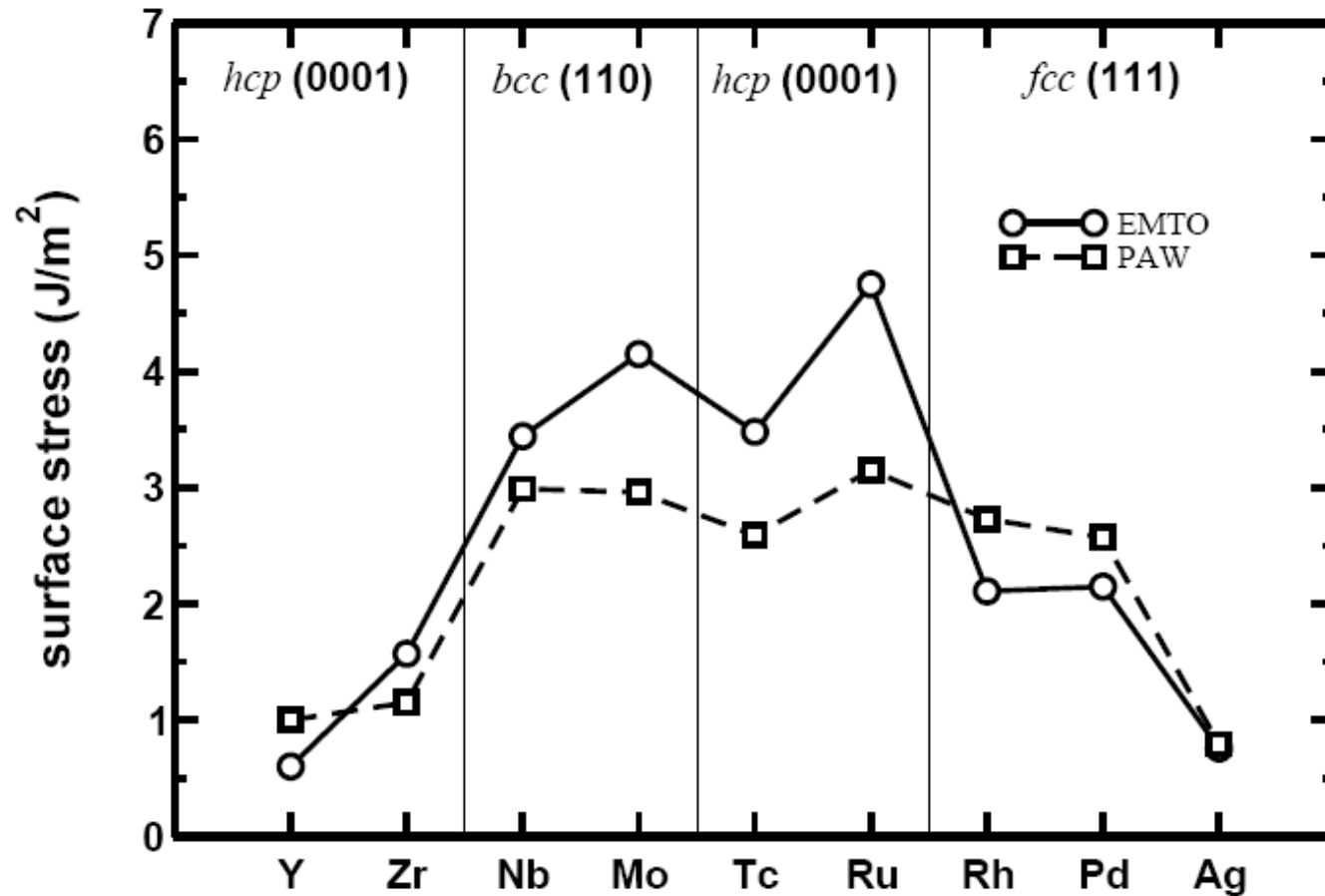


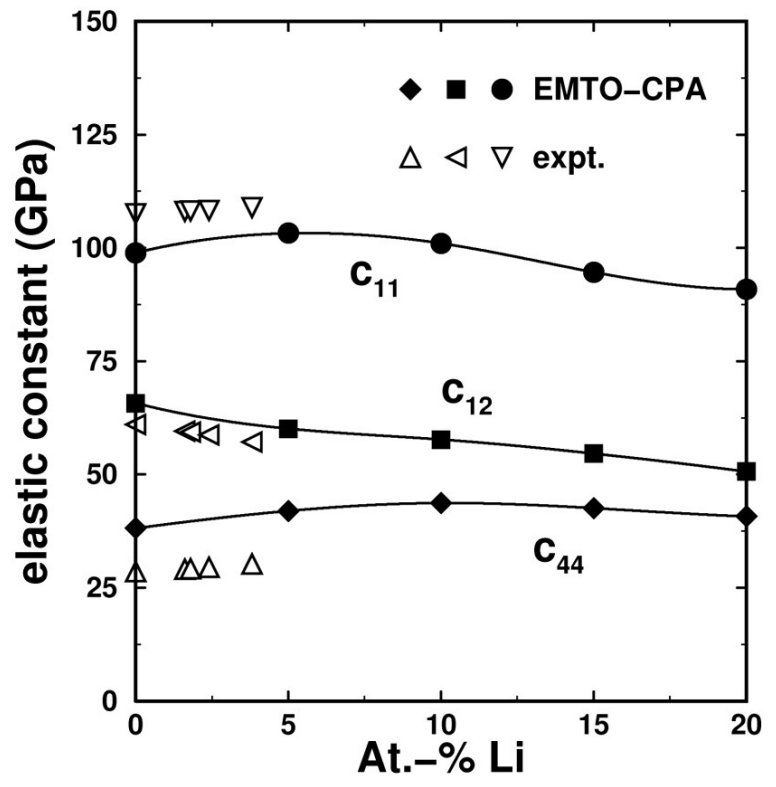
Fig. 7.7. Theoretical surface stress for the close-packed surfaces of 4d transition metal. Solid and dashed lines represent EMTO and PAW [168] results, respectively.

**Demonstration**

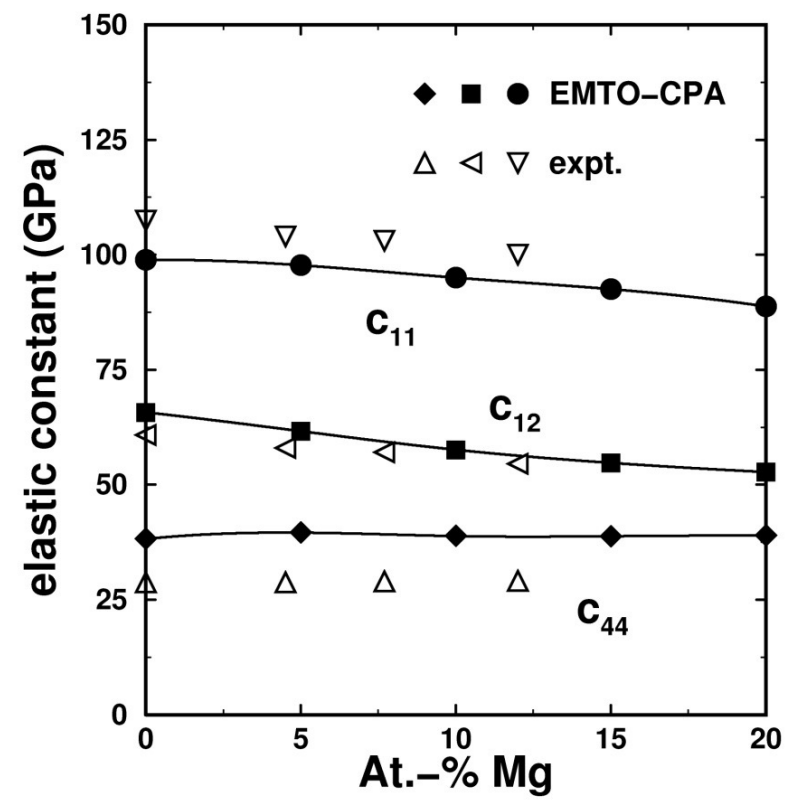
**Alloys**

# Elastic properties

### Al-Li solid-solution



### Al-Mg solid-solution



# Elastic properties

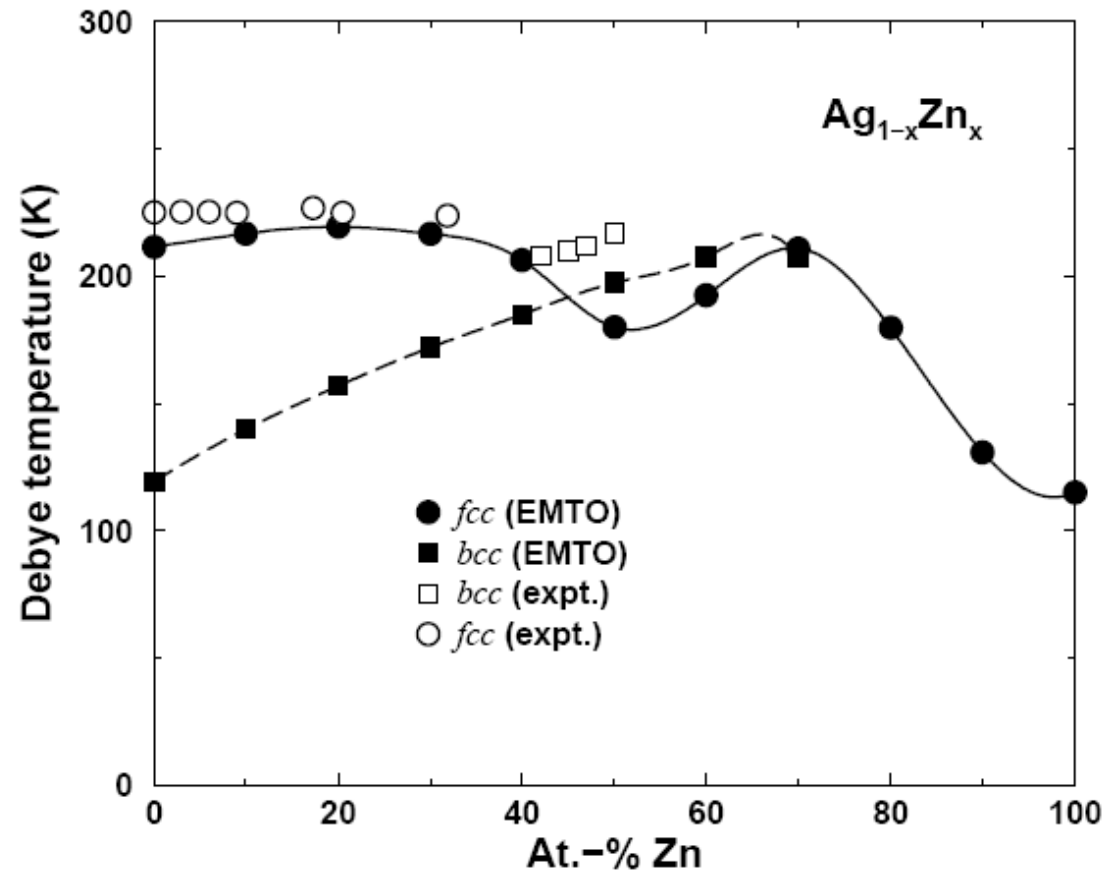


Fig. 8.18. The low temperature theoretical (EMTO-LDA) and experimental [239, 244] Debye temperatures of  $Ag_{1-x}Zn_x$  random alloys in the *fcc* and *bcc* crystallographic phases [115].

# Crystal structure, transformations

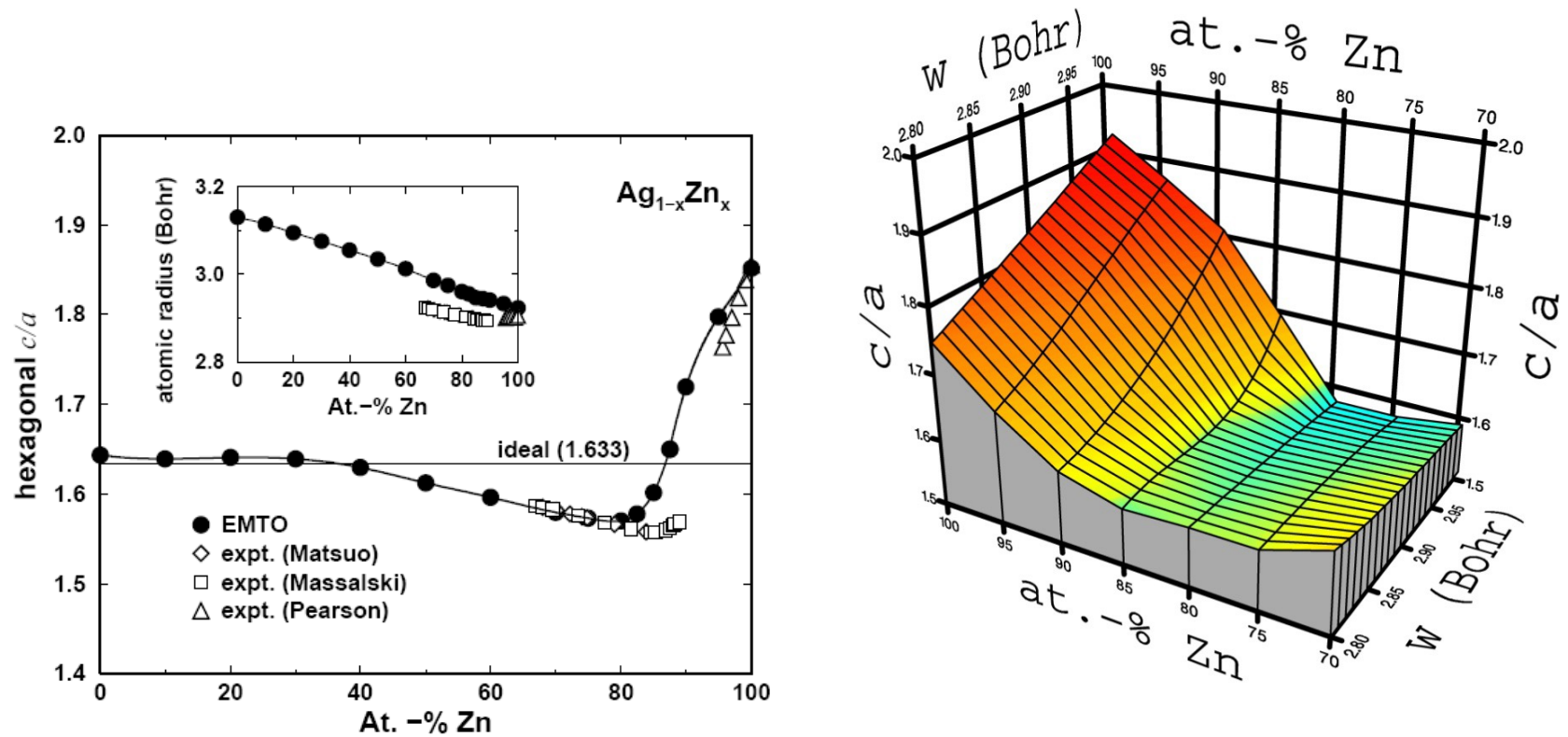
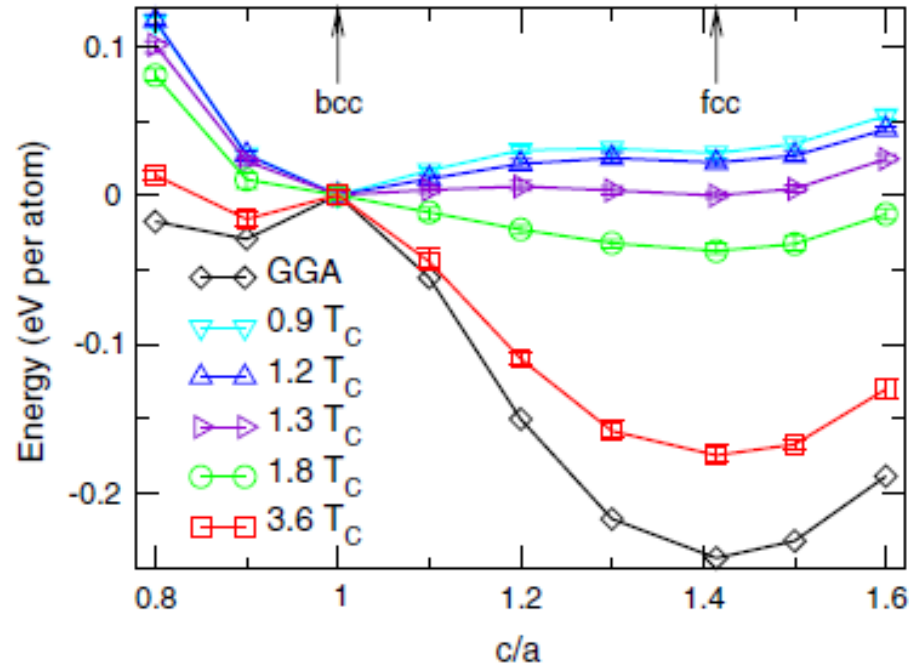


Fig. 8.19. Concentration dependence of the theoretical (EMTO-GGA) equilibrium axial ratio  $(c/a)_0$  in *hcp*  $\text{Ag}_{1-x}\text{Zn}_x$  alloys. The inset shows the calculated equilibrium atomic radii  $w$  as a function of Zn content. Experimental data are from Matsuo [248], Massalski [247] and Pearson [232].

# Paramagnetic Fe



PHYSICAL REVIEW B 79, 094111 (2009)

Effect of magnetic state on the  $\gamma$ - $\alpha$  transition in iron: First-principles calculations of the Bain transformation path

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(Received 14 September 2008; revised manuscript received 23 February 2009; published 24 March 2009)

PRL 106, 106405 (2011)

PHYSICAL REVIEW LETTERS

week ending  
11 MARCH 2011

## Electronic Correlations at the $\alpha$ - $\gamma$ Structural Phase Transition in Paramagnetic Iron

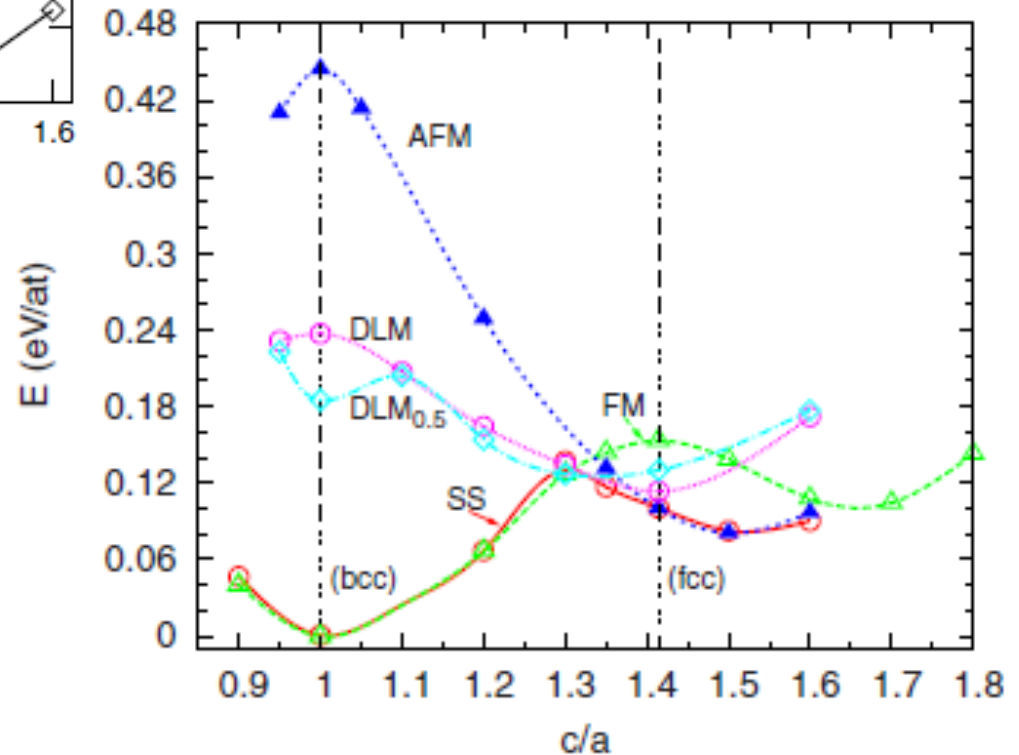
I. Leonov,<sup>1</sup> A. I. Poteryaev,<sup>2,3</sup> V. I. Anisimov,<sup>2</sup> and D. Vollhardt<sup>1</sup>

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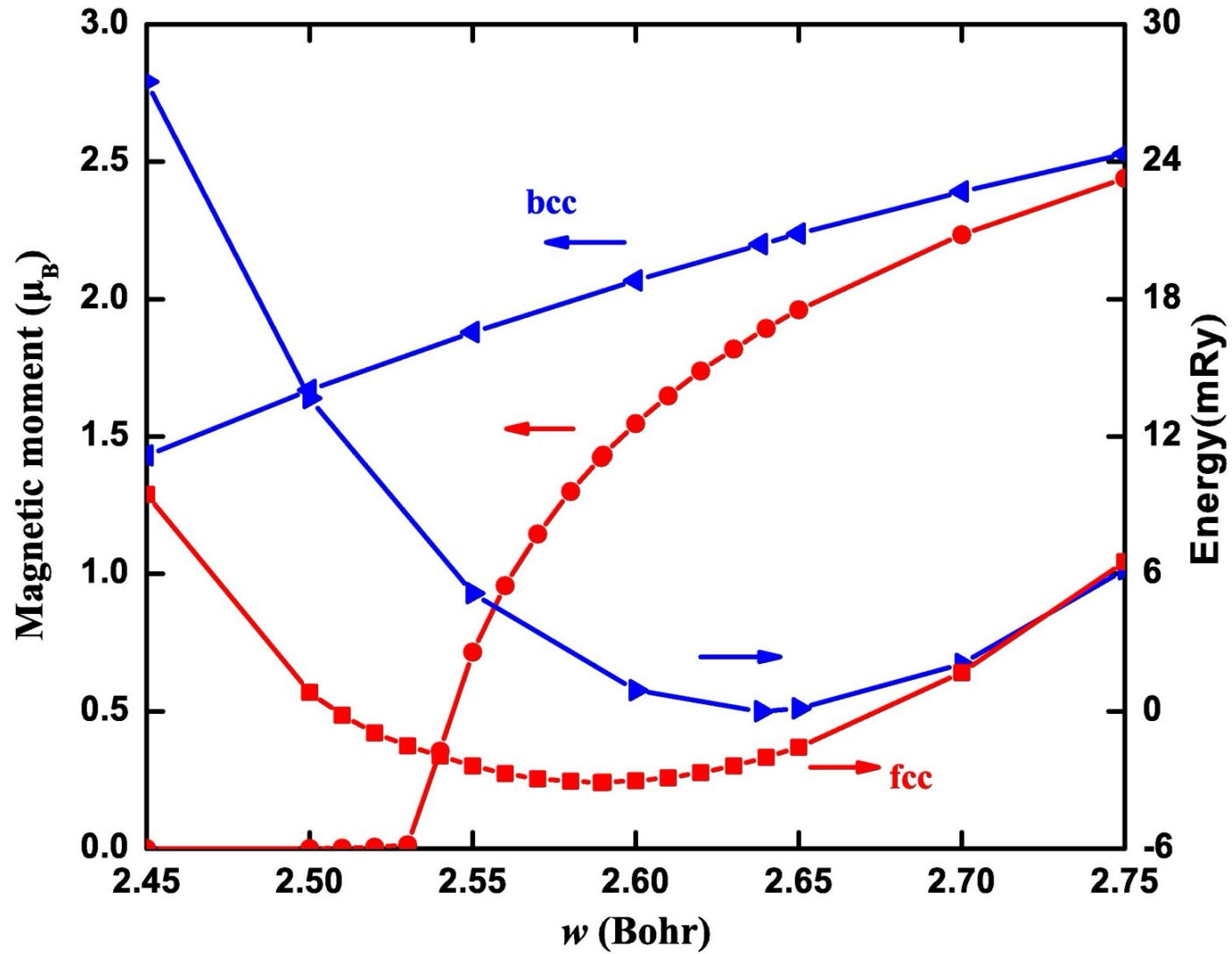
<sup>2</sup>Institute of Metal Physics, Sofia Kovalevskaya Street 18, 620219 Yekaterinburg GSP-170, Russia

<sup>3</sup>Institute of Quantum Materials Science, 620107 Yekaterinburg, Russia  
(Received 25 August 2010; published 11 March 2011)

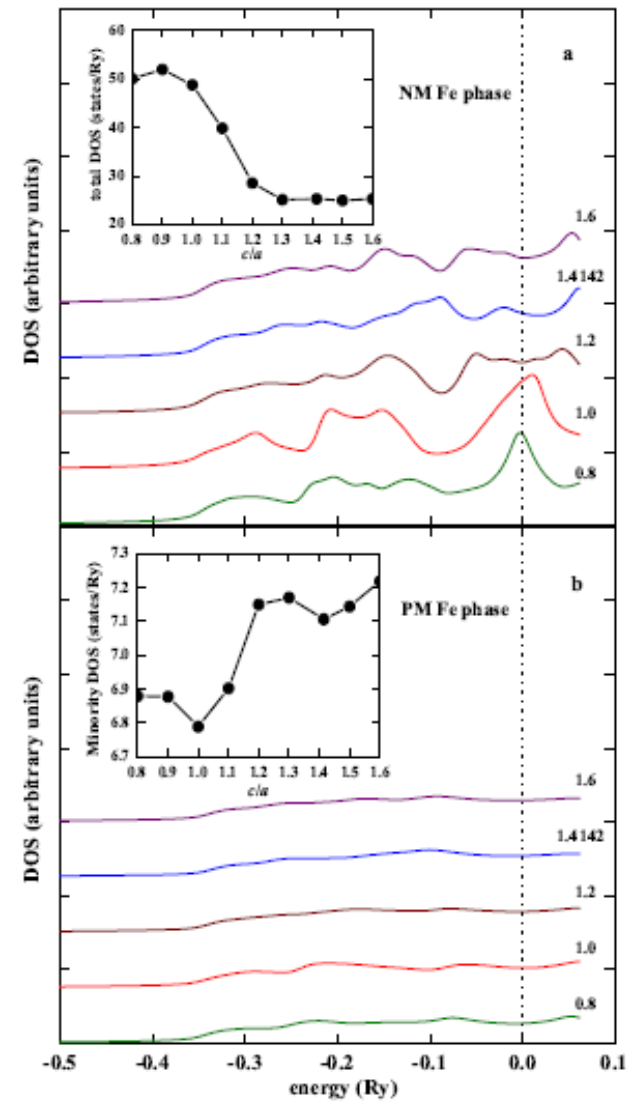
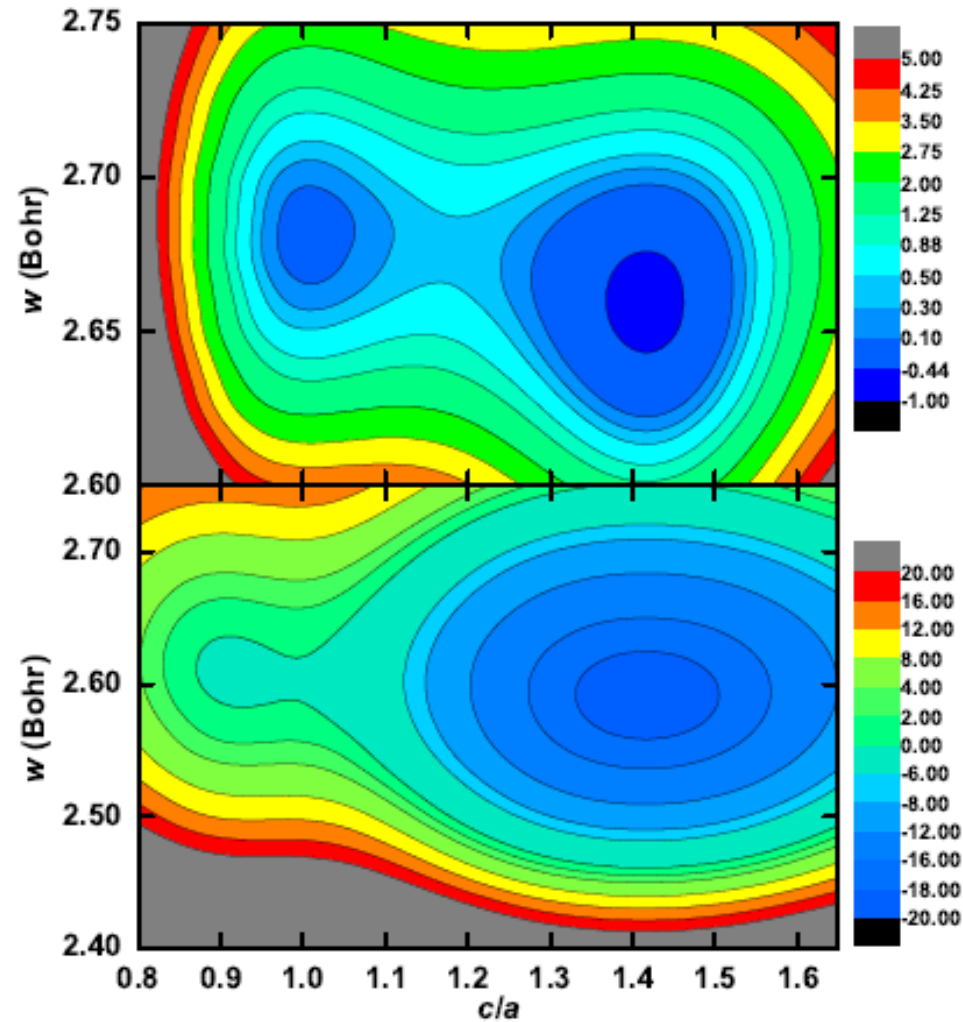
We compute the equilibrium crystal structure and phase stability of iron at the  $\alpha$ (bcc) -  $\gamma$ (fcc) phase transition as a function of temperature, by employing a combination of *ab initio* methods for calculating electronic band structures and dynamical mean-field theory. The magnetic correlation energy is found to be an essential driving force behind the  $\alpha$ - $\gamma$  structural phase transition in paramagnetic iron.



# Paramagnetic Fe



# Paramagnetic Fe

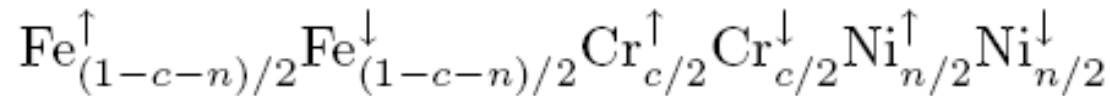




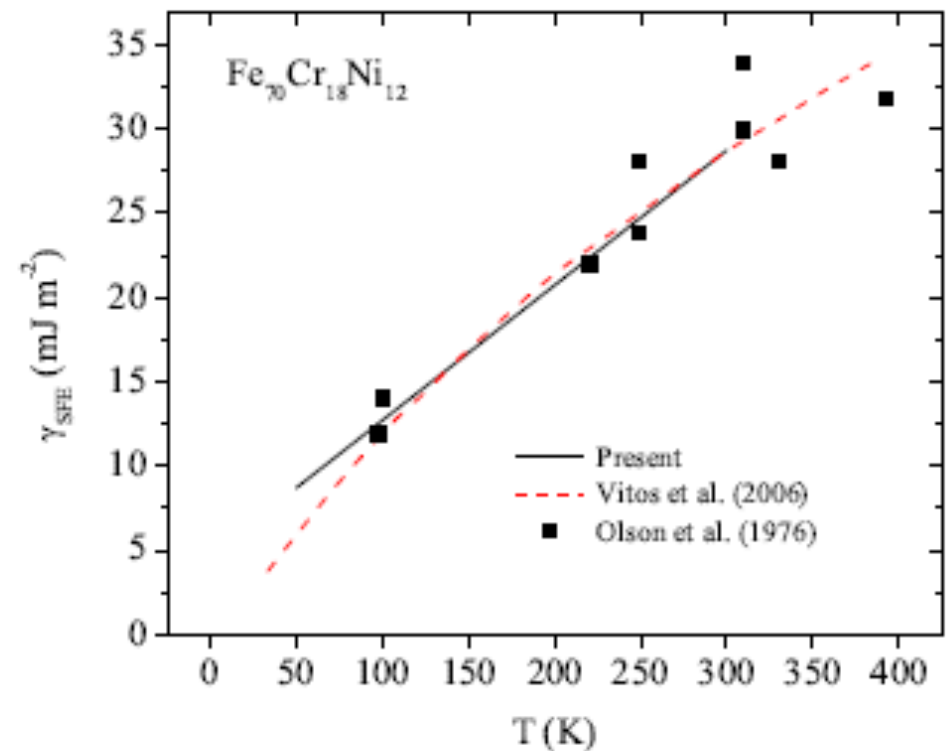
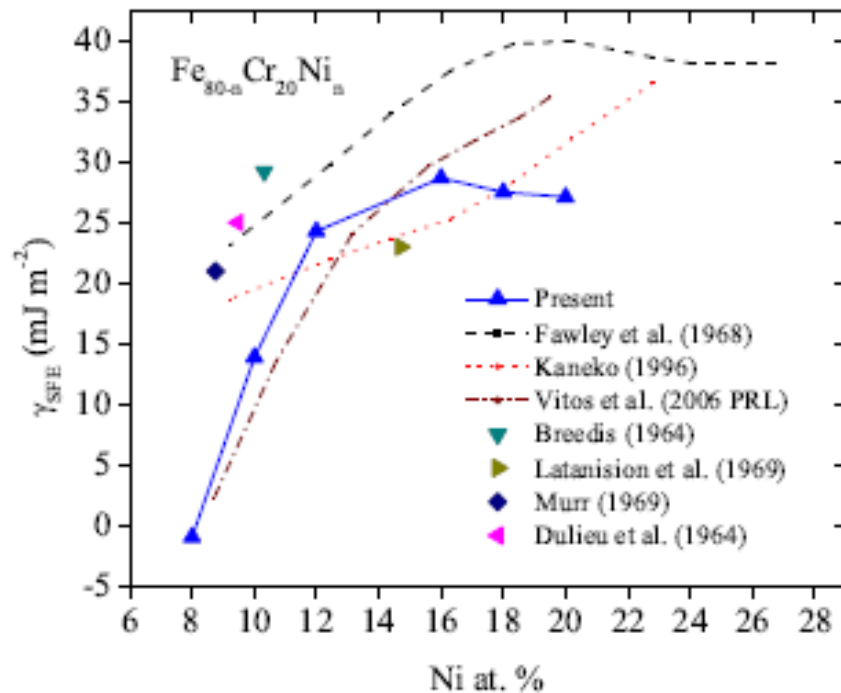
# Paramagnetic FeCrNi alloys (stainless steel) Stacking-fault energy



	$V$	$c_{11}$	$c_{12}$	$c_{44}$	$A$	$B$	$G$	$B/G$
EMTO	78.93	208.6	143.5	132.8	4.07	165.2	77.3	2.13
expt.	79.45	204.6	137.7	126.2	3.78	158.2	77.4	2.04
$\Delta$	-0.6	2.0	4.2	5.2	7.6	4.4	-0.1	4.4



- paramagnetic metals
- $T_{\text{mag}} \sim 50\text{-}100\text{ K}$
- fcc structure



# High Entropy Alloys

## Ab initio investigation of high-entropy alloys of 3d elements

Fuyang Tian,<sup>1,2</sup> Lajos Karoly Varga,<sup>3</sup> Nanxian Chen,<sup>2,4</sup> Lorand Delczeg,<sup>1</sup> and Levente Vitos<sup>1,3,5</sup>

<sup>1</sup>Applied Materials Physics, Department of Materials Science and Engineering, Royal Institute of Technology, Stockholm SE-100 44, Sweden

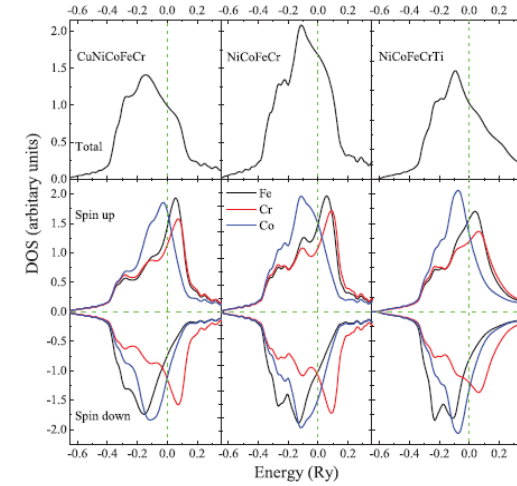
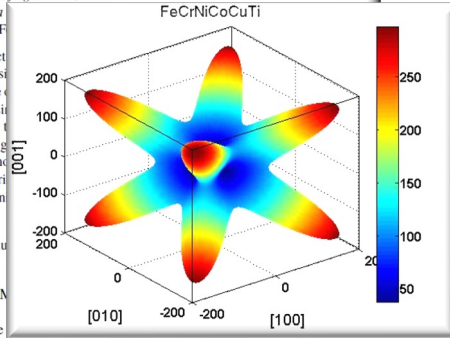
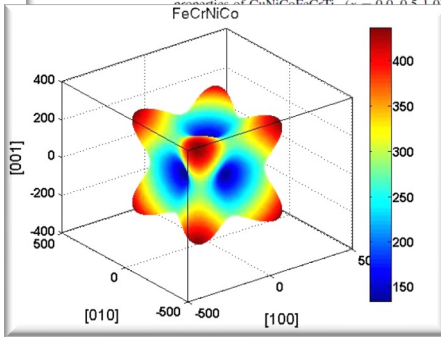
<sup>2</sup>Institute for Applied Physics, University of Science and Technology Beijing, Beijing 100083, China

<sup>3</sup>Wigner Research Centre for Physics, Institute for Solid State Physics and Optics, H-1525 Budapest, P.O. Box 49, Hungary

<sup>4</sup>Department of Physics, Tsinghua University, Beijing 100084, China

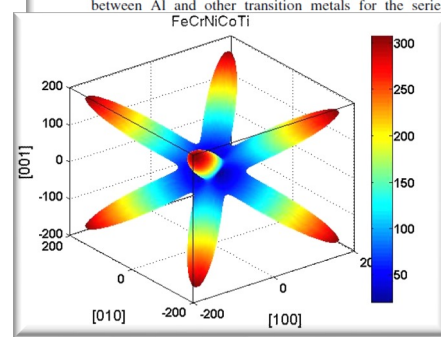
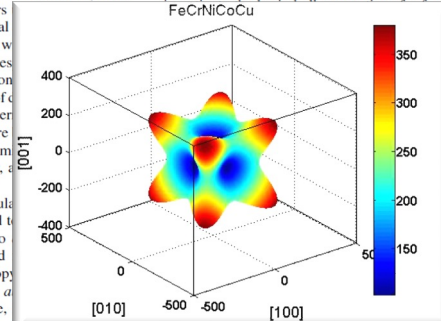
<sup>5</sup>Department of Physics and Astronomy, Division of Materials Theory, Uppsala University, Uppsala, Sweden  
(Received 26 October 2012; published 26 February 2013)

Single-phase high-entropy alloys are investigated using the exact combination with the coherent potential approximation (CPA). Choosing NiCoFeCr alloy as an example, we compare the CPA results with those from the equilibrium Wigner-Seitz radius and elastic properties, the simulation results with the SC approach. Next, we employ the CPA to investigate NiCoFeCrTi and NiCoFeCrTiTi high-entropy alloys. The CPA results are compared with the experimental data demonstrating that the CPA is a powerful tool for the design of a new class of engineering materials with properties superior to those of the Ti-containing alloys.



High-entropy alloys (HEAs) have attracted rapidly increasing attention in the scientific community.<sup>1–26</sup> In the experimental area, researchers including traditional casting, mechanical alloying and splat quenching, to obtain the HEAs with unique mechanical, thermal, and electronic properties. With the appearance of a large number of HEAs, one could establish general rules governing HEAs. Such empirical assessments were based on solution theory, and made use of the atomistic simulation theory, and made use of the atomistic simulation theory, and made use of the atomistic simulation theory.

On the other hand, atomistic simulation theory applied to study the features connected with the HEAs. For instance, del Grosso and Bozzolo-Ferrante-Smith (BFS) method investigate the transition to the high-entropy alloy with refractory elements.<sup>24</sup> Based on the atomistic simulation theory, the body-centered-cubic (bcc) phase has been found to be stable for the series of HEAs.



and CoFeMnNiTi.<sup>26</sup> Despite the fact that HEAs, it is particularly difficult to use conventional *ab initio* atomistic simulation methods to investigate these systems. That is because HEAs are chemically and often also magnetically disordered multicomponent extended solid solutions. In the present work, our primary goal is to assess the performance of standard alloy theory based on *ab initio* density functional theory<sup>27,28</sup> in the case of HEAs. To this end, we employ the exact muffin-tin orbitals (EMTO) method<sup>29–34</sup> in combination with the coherent potential approximation (CPA)<sup>35</sup> to investigate the

of the alloy components. According to that, the constituent elements are specified in order of their atomic numbers, starting from the element having the largest atomic number according to this convention, it is possible to put the common minor elements (e.g., Ti or Al) to the end of the chemical formula.

PERIODIC TABLE  
Atomic Properties of the Elements

Physics Laboratory NIST Standard Reference Data Program  
physics.nist.gov www.nist.gov www.nist.gov/ia

U.S. DEPARTMENT OF COMMERCE  
Technology Administration  
National Institute of Standards and Technology

Frequently used fundamental physical constants  
For the most accurate values of these and other constants, visit [physics.nist.gov/constants](http://physics.nist.gov/constants)  
1 second = 9 192 631 770 periods of radiation corresponding to the transition between the two hyperfine levels of the ground state of <sup>133</sup>Cs  
speed of light in vacuum  $c$  299 792 458 m s<sup>-1</sup> (exact)  
Planck constant  $h$  6.626 069 3 × 10<sup>-34</sup> J s  
elementary charge  $e$  1.602 176 634 × 10<sup>-19</sup> C  
electron mass  $m_e$  9.109 382 91 × 10<sup>-31</sup> kg  
proton mass  $m_p$  1.672 621 63 × 10<sup>-27</sup> kg  
fine-structure constant  $\alpha$  7.297 352 569 8 × 10<sup>-3</sup>  
Rydberg constant  $R_\infty$  1.097 373 157 × 10<sup>7</sup> m<sup>-1</sup>  
Bohr radius  $a_0$  5.291 772 109 × 10<sup>-11</sup> m  
Boltzmann constant  $k_B$  1.380 658 × 10<sup>-23</sup> J K<sup>-1</sup>

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
H	He	Li	Be	B	C	N	O	F	Ne	Na	Mg	Al	Si	P	S	Cl	Ar
19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72
Cs	Ba	La	Ce	Pr	Nd	Pm	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb	Lu	
87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	
Fr	Ra	Ac	Th	Pa	U	Np	Pu	Am	Cm	Bk	Cf	Es	Fm	Md	No	Lr	

Legend:  
Solids (blue)  
Liquids (green)  
Gases (red)  
Artificially Prepared (yellow)

For a description of the atomic data, visit [physics.nist.gov/atomic/](http://physics.nist.gov/atomic/)

March 1999

Structural stability of NiCoFeCrAl<sub>x</sub> high-entropy alloy from *ab initio* theory

Fuyang Tian,<sup>1,2</sup> Lorand Delczeg,<sup>1</sup> Nanxian Chen,<sup>2,3</sup> Lajos Karoly Varga,<sup>4</sup> Jiang Shen,<sup>2</sup> and Levente Vitos<sup>1,4,5</sup>

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<sup>4</sup>Wigner Research Centre for Physics, Institute for Solid State Physics and Optics, H-1525 Budapest, P.O. Box 49, Hungary

<sup>5</sup>Department of Physics and Astronomy, Division of Materials Theory, Uppsala University, Box 516, SE-751210, Uppsala, Sweden

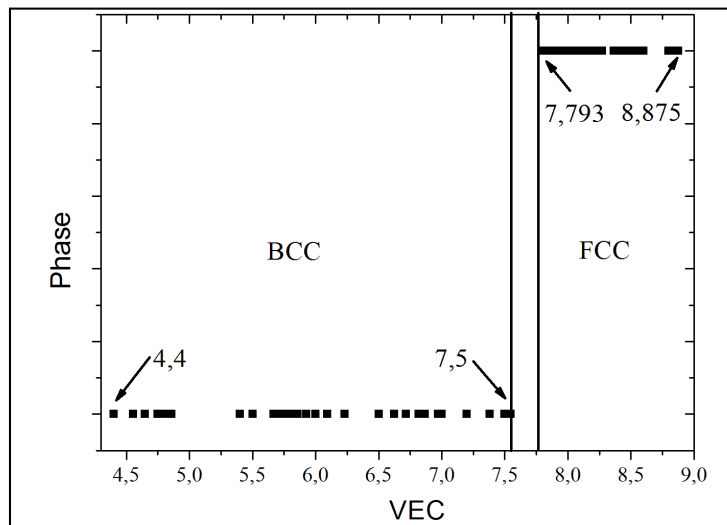
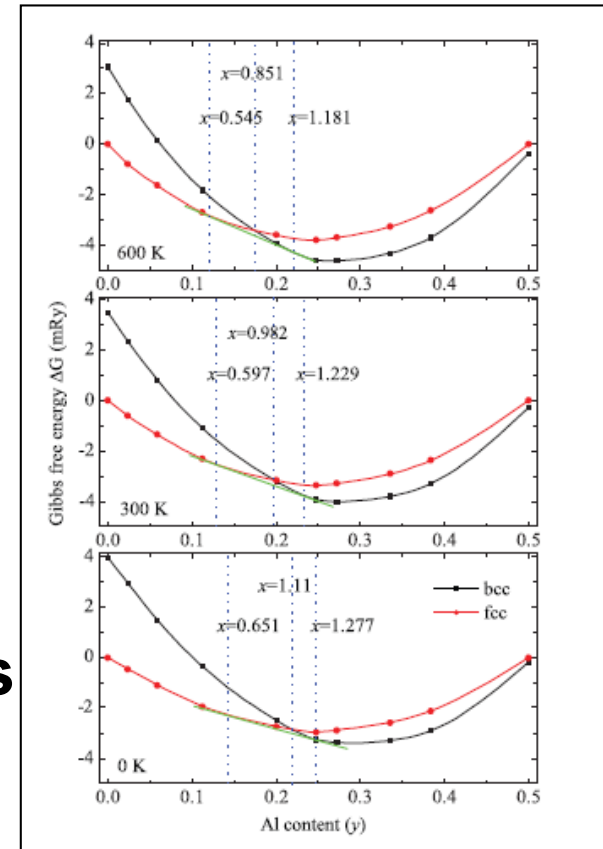
(Received 2 April 2013; published xxxxx)

First-principles alloy theory predicts that at room temperature the paramagnetic NiCoFeCrAl<sub>x</sub> high entropy alloys adopt the face centered cubic (fcc) structure for  $x \lesssim 0.60$  and the body centered cubic (bcc) structure for  $x \gtrsim 1.23$ , with an fcc-bcc duplex region in between the two pure phases. The calculated single- and polycrystal elastic parameters exhibit strong composition and crystal structure dependence. Based on the present theoretical findings, it is concluded that alloys around the equimolar NiCoFeCrAl composition have superior mechanical performance as compared to the single-phase regions.

DOI: 10.1103/PhysRevB.00.005100

PACS number(s): 62.20.D-, 71.20.Be, 81.05.Bx

# Theoretical and experimental phase boundaries in NiCoFeCrAl<sub>x</sub>-based HEAs



	Al <sub>x</sub> CrFeCoNi		Al <sub>x</sub> CrMnFeCoNi	
	fcc	bcc	fcc	bcc
<b>x</b>	<b>0.651</b>	<b>1.277</b>	<b>0.488</b>	<b>1.658</b>
<b>c<sub>Al</sub> (%)</b>	<b>13.4</b>	<b>24.2</b>	<b>8.9</b>	<b>24.9</b>
<b>VEC</b>	<b>7.52</b>	<b>6.98</b>	<b>7.56</b>	<b>6.75</b>





### *Ab initio* design of elastically isotropic TiZrNbMoV<sub>x</sub> high-entropy alloys



Fuyang Tian<sup>a,b,\*</sup>, Lajos Karoly Varga<sup>c</sup>, Nanxian Chen<sup>b,d</sup>, Jiang Shen<sup>b</sup>, Levente Vitos<sup>a,c,e</sup>

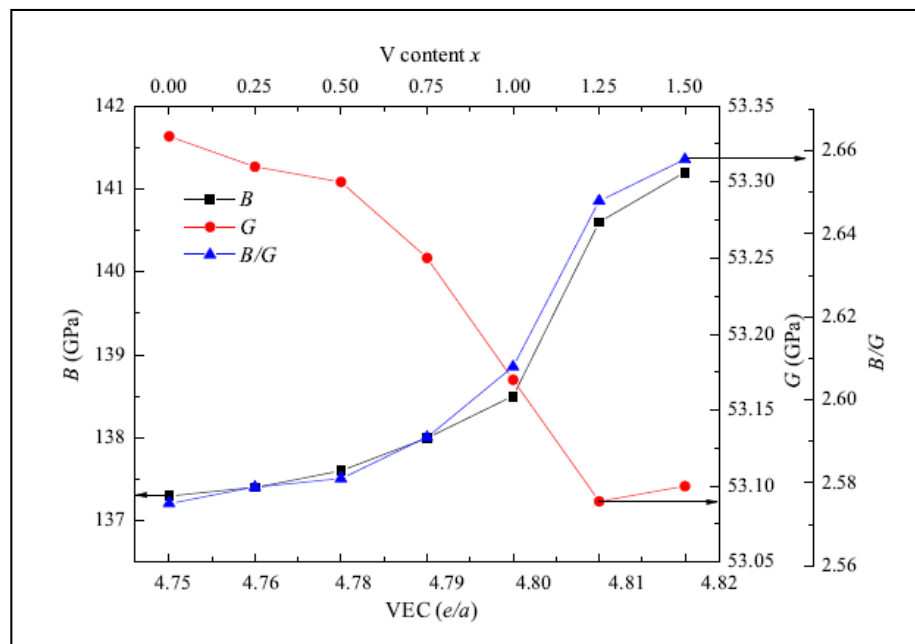
<sup>a</sup> Applied Materials Physics, Department of Materials Science and Engineering, Royal Institute of Technology, Stockholm, Sweden

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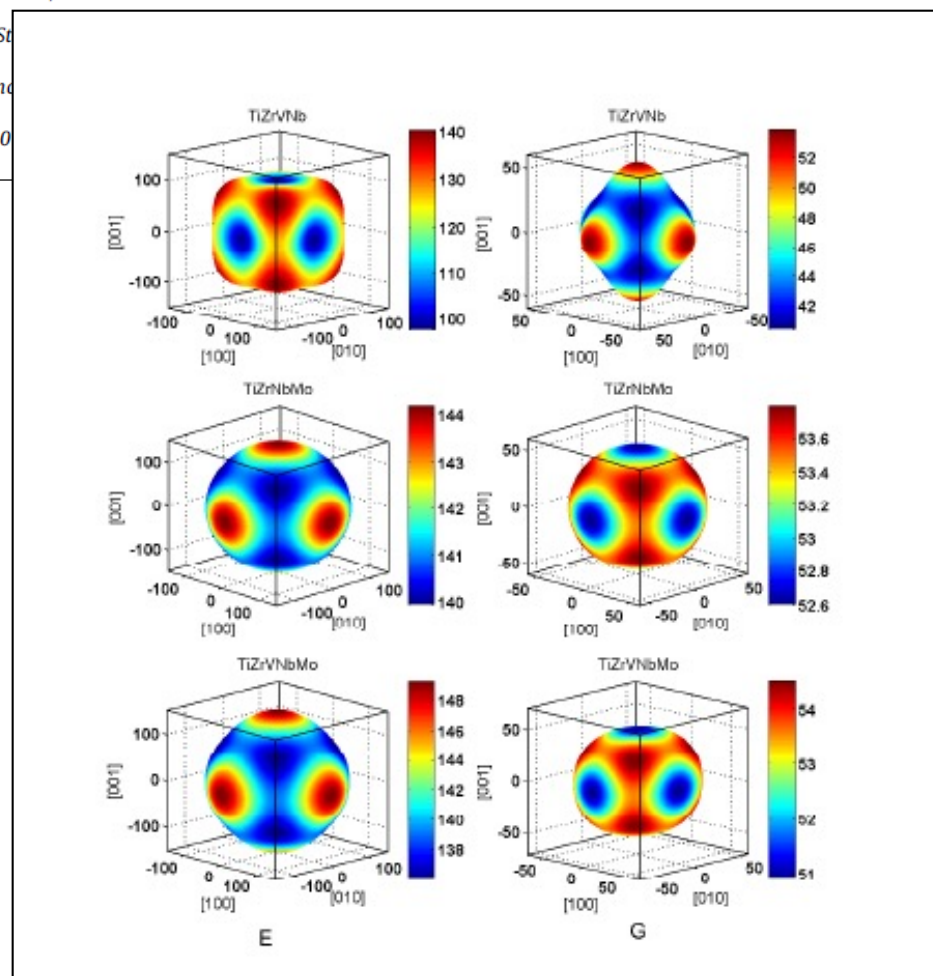
<sup>c</sup> Institute for Solid State Physics and Optics, Wigner Research Centre for Physics, Hungarian Academy of Sciences, Budapest, Hungary

<sup>d</sup> Department of Physics, Tsinghua University, Beijing 100084, China

<sup>e</sup> Department of Physics and Astronomy, Division of Materials Theory, Uppsala University, Box 516, SE-751210, Sweden



**Theoretical prediction**



# EMTO-CPA versus VASP-SQS



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## Alloying effect on the elastic properties of refractory high-entropy alloys



Li-Yun Tian<sup>a,b</sup>, Guisheng Wang<sup>c</sup>, Joshua S. Harris<sup>d</sup>, Douglas L. Irving<sup>d</sup>,  
Jijun Zhao<sup>b</sup>, Levente Vitos<sup>a,e,f</sup>

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<sup>b</sup>Key Laboratory of Materials Modification by Laser, Ion, and Electron Beams of Ministry of Education, Dalian University of Technology, Dalian 116024, China

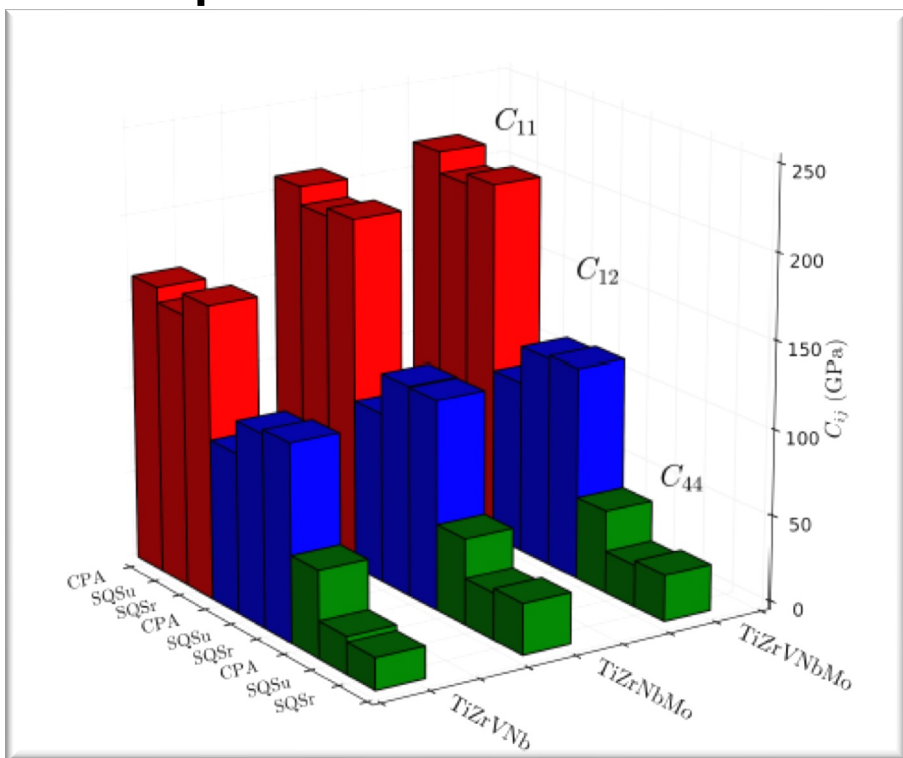
<sup>c</sup>School of Applied Mathematics and Physics, Beijing University of Technology, Beijing 100124, China

<sup>d</sup>Department of Materials Science and Engineering, North Carolina State University, Raleigh, NC 27695-7907, United States

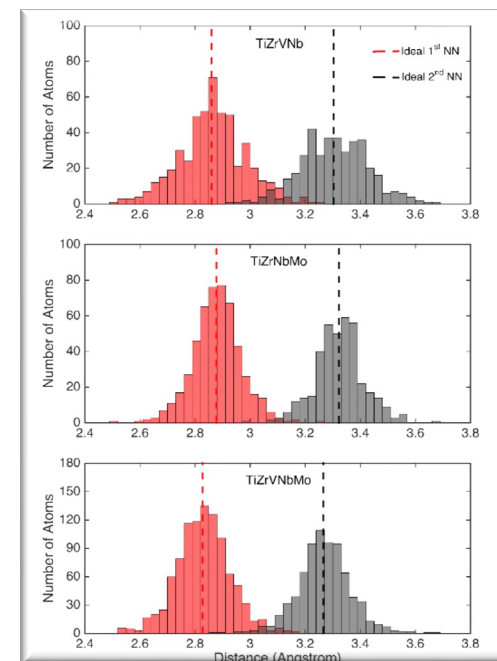
<sup>e</sup>Department of Physics and Astronomy, Division of Materials Theory, Uppsala University, Box 516, SE-75121 Uppsala, Sweden

<sup>f</sup>Research Institute for Solid State Physics and Optics, Wigner Research Center for Physics, P.O. Box 49, Budapest H-1525, Hungary

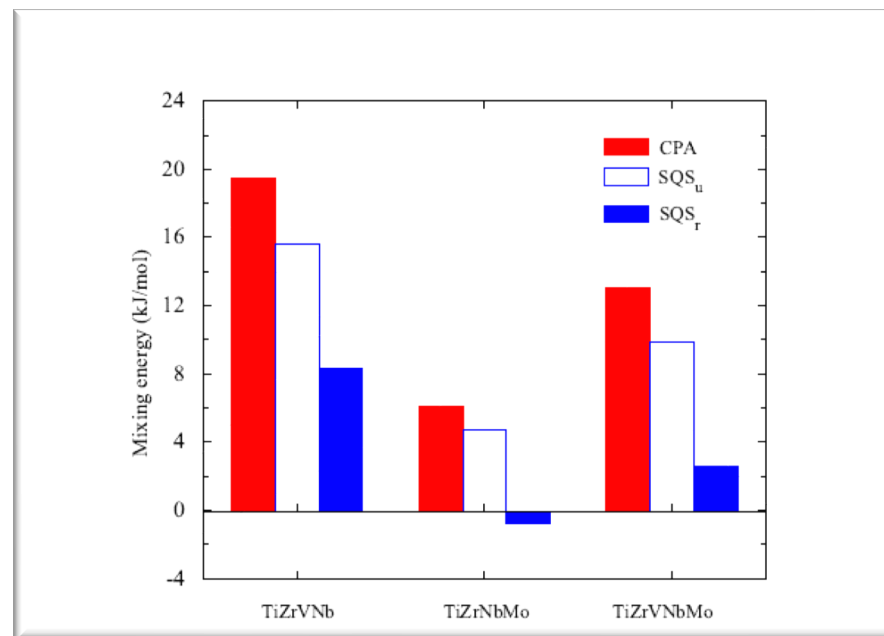
### Elastic parameters



### LLD histograms VASP-SQS (bcc NN)



### Mixing energy



# Magnetism in HEAs



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## Mechanism of magnetic transition in FeCrCoNi-based high entropy alloys



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Modeling based on Heisenberg Hamiltonian in combination with ab initio magnetic exchange parameters

$$H = - \sum_{i,j} J_{ij} \mathbf{m}_i \cdot \mathbf{m}_j,$$

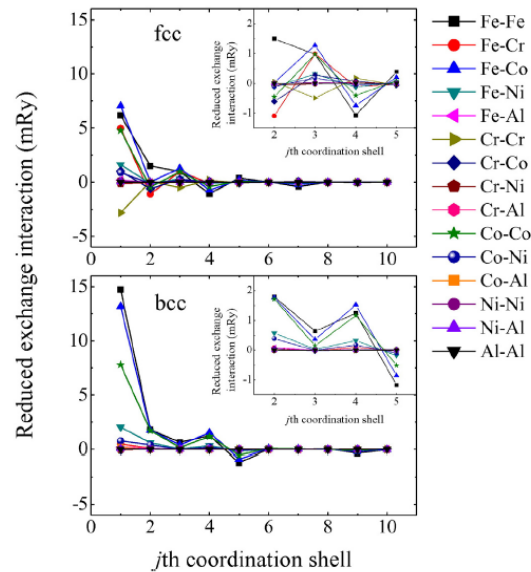
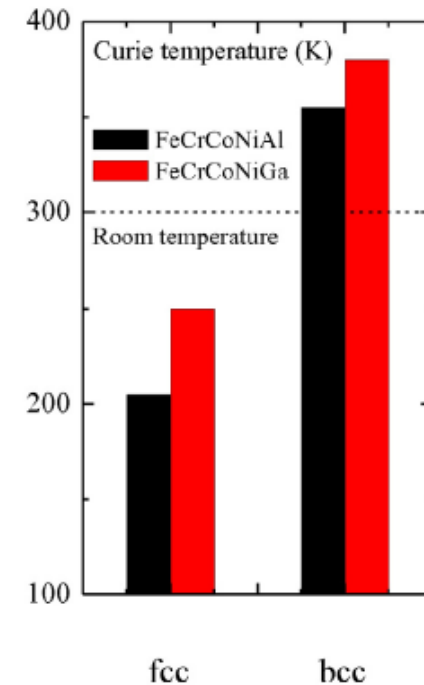
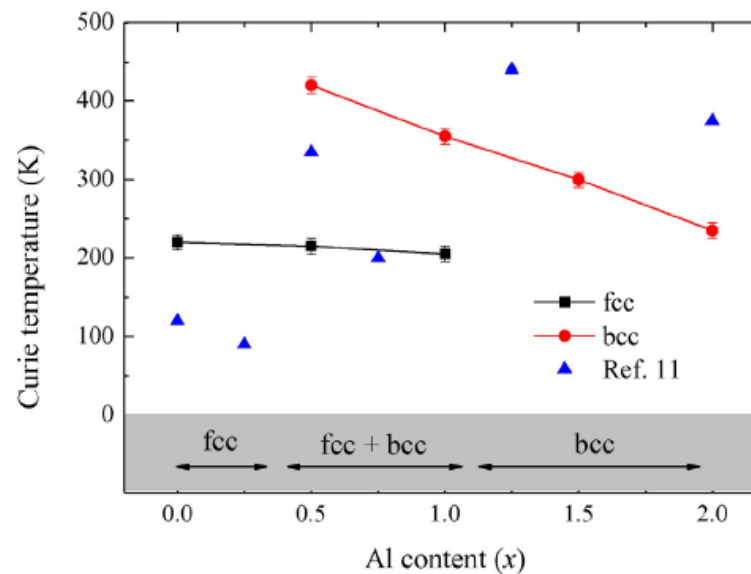


Fig. 2. Magnetic exchange interactions for equiatomic FeCrCoNiAl as a function of the coordination shell for fcc and bcc phases, respectively.







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Intermetallics

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## Mapping the magnetic transition temperatures for medium- and high-entropy alloys

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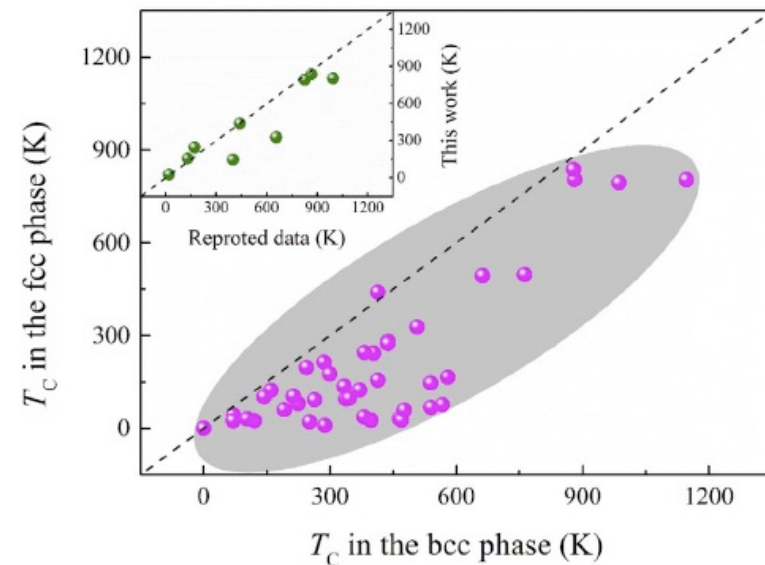
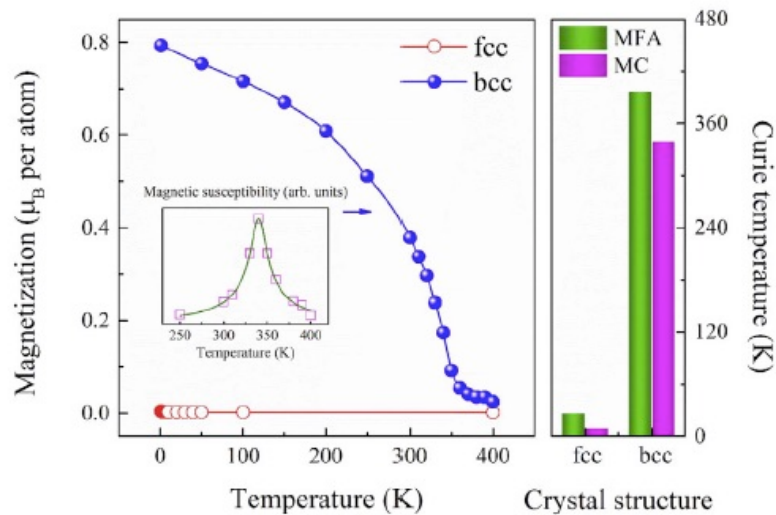
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OPEN

## Thermal spin fluctuations in CoCrFeMnNi high entropy alloy

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High entropy alloys based on 3d transition metals display rich and promising magnetic characteristics for various high-technology applications. Understanding their behavior at finite temperature is, however, limited by the incomplete experimental data for single-phase alloys. Here we use first-principles alloy theory to investigate the magnetic structure of polymorphic CoCrFeMnNi in the paramagnetic state by accounting for the longitudinal spin fluctuations (LSFs) as a function of temperature. In both face-centered cubic (fcc) and hexagonal close-packed (hcp) structures, the LSFs induce sizable magnetic moments for Co, Cr and Ni. The impact of LSFs is demonstrated on the phase stability, stacking fault energy and the fcc-hcp interfacial energy. The hcp phase is energetically preferable to the fcc one at cryogenic temperatures, which results in negative stacking fault energy at these conditions. With increasing temperature, the stacking fault energy increases, suppressing the formation of stacking faults and nano-twins. Our predictions are consistent with recent experimental findings.

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## Thermal spin fluctuation effect on the elastic constants of paramagnetic Fe from first principles

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## Elastic properties of paramagnetic austenitic steel at finite temperature: Longitudinal spin fluctuations in multicomponent alloys

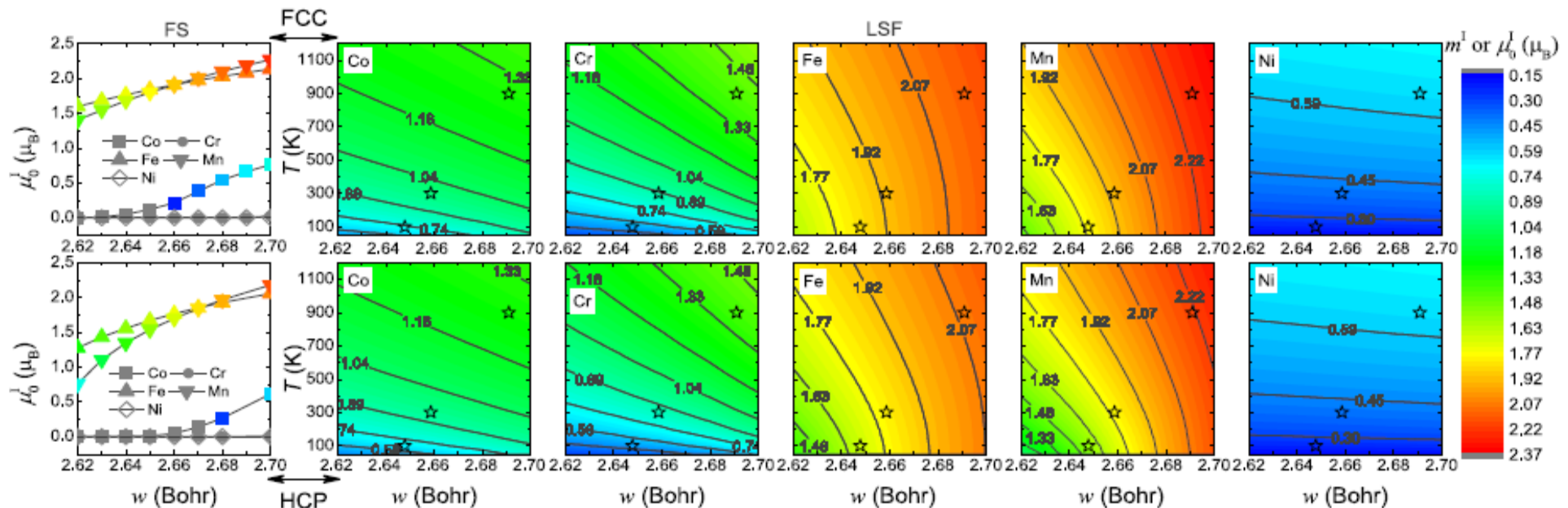
Zhihua Dong,<sup>1,\*</sup> Stephan Schönecker,<sup>1,†</sup> Dengfu Chen,<sup>2</sup> Wei Li,<sup>1</sup> Mujun Long,<sup>2</sup> and Levente Vitos<sup>1,3,4</sup>

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## Thermal expansion in FeCrCoNiGa high-entropy alloy from theory and experiment

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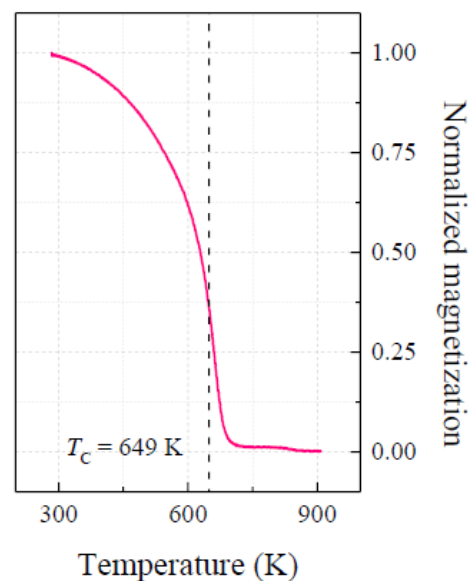
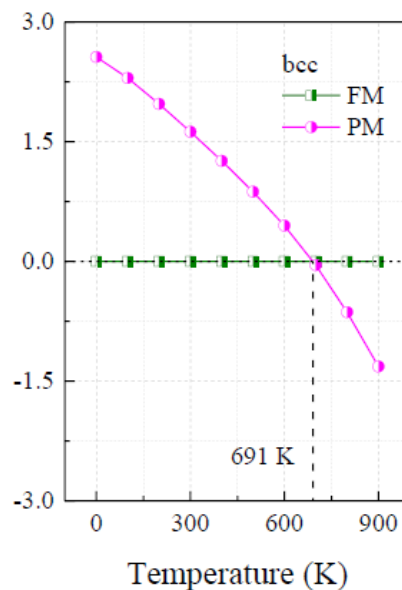
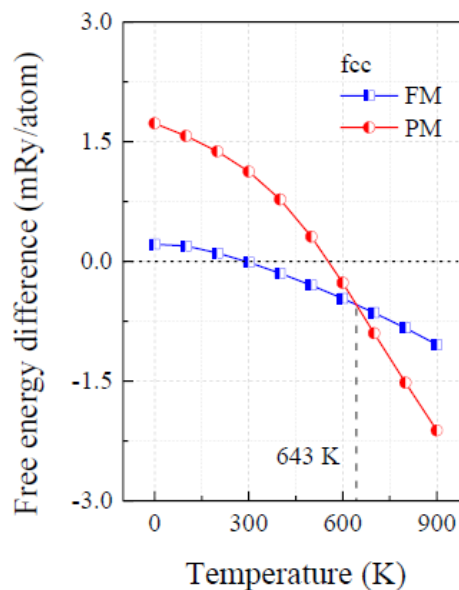
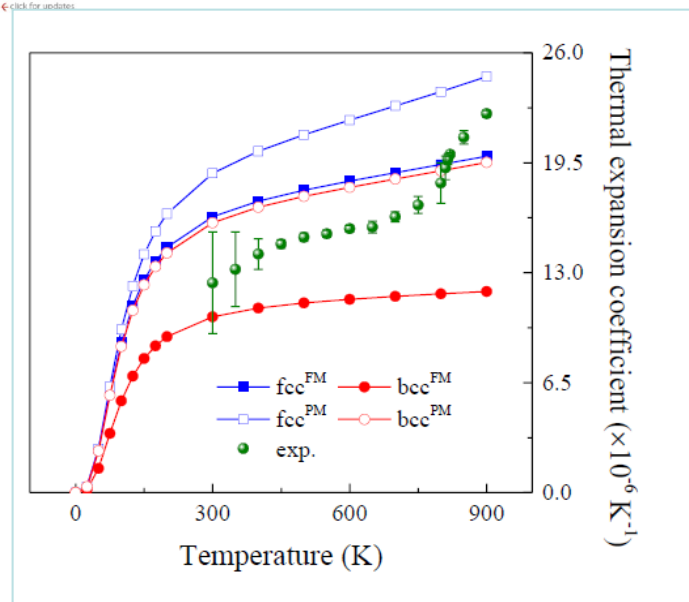
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## Strengthening Induced by MagnetoChemical Transition in Al-Doped Fe-Cr-Co-Ni High-Entropy Alloys


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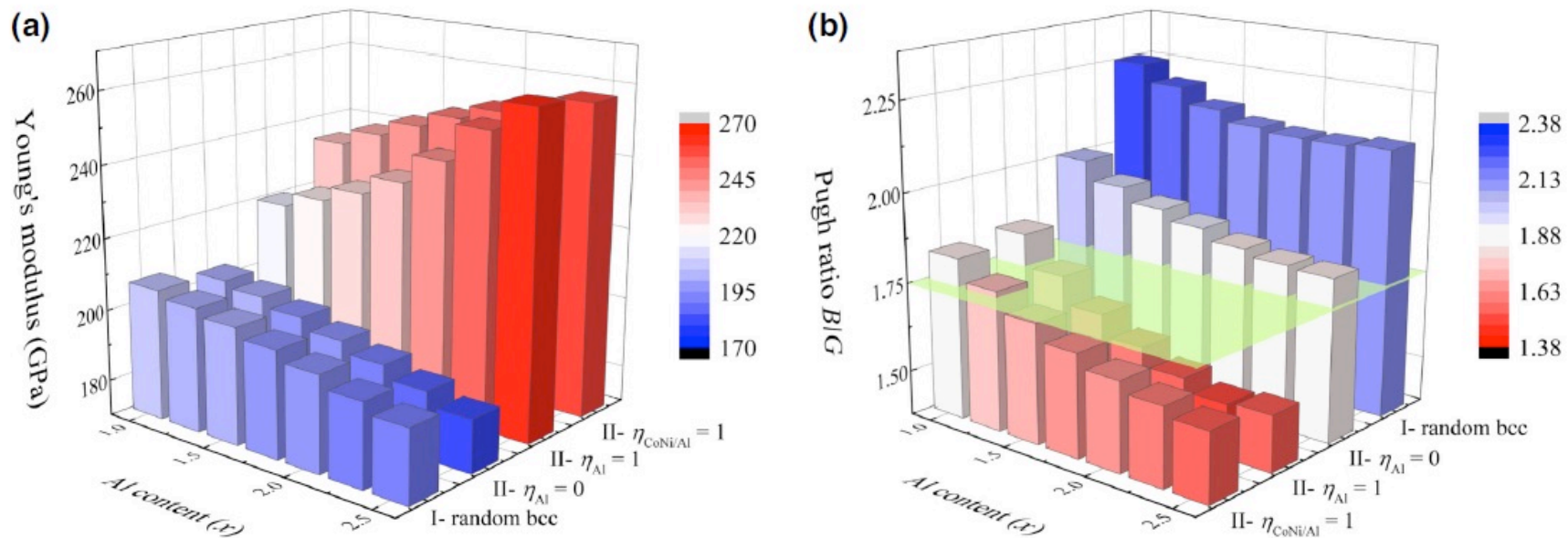
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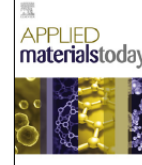


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## High entropy alloys: Substituting for cobalt in cutting edge technology

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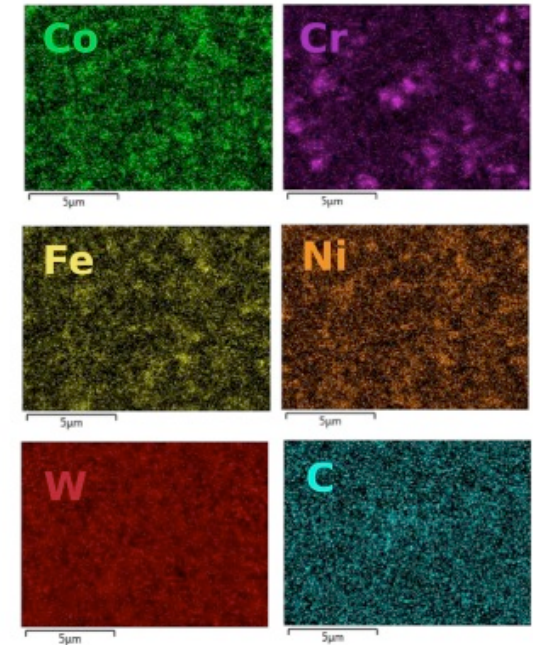
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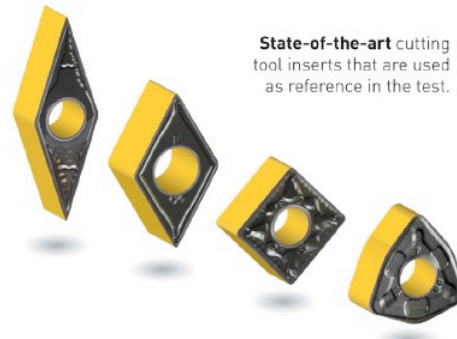
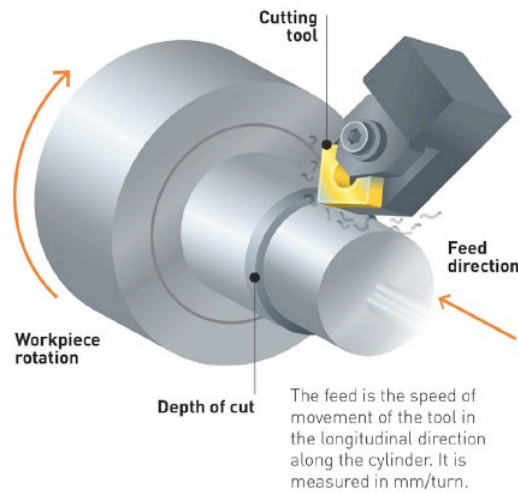


### TURNING TEST

#### SCHEMATIC VIEW OF THE MACHINE TEST

The **depth-of-cut** is radial difference between the part of the cylinder that has been cut and the untouched surface.

In the test, the feed is **0.7mm/turn** and the depth-of-cut is **2mm**.



State-of-the-art cutting tool inserts that are used as reference in the test.

The graph shows the resulting edge deformations of the cutting tools after 30 s of turning at different turning speeds.

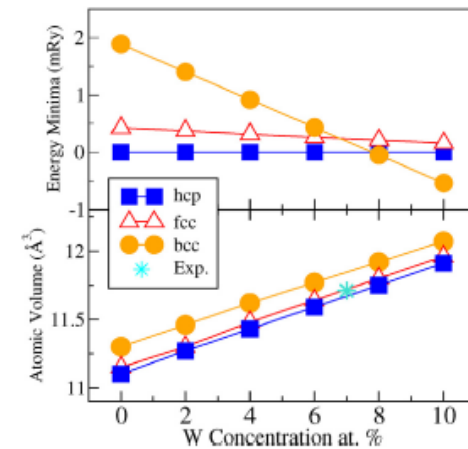
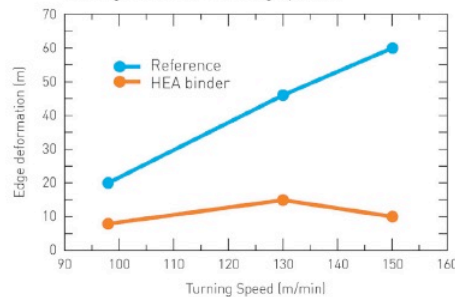


Fig. 5. A schematic view of the machine test, the results of the HEA bonded product compared to a state-of-the-art reference with Co as binder phase. The actual shape of the tested inserts is the third from the top.

# Plasticity, stacking fault energy of HEAs

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Scripta Materialia

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## Temperature dependent stacking fault energy of FeCrCoNiMn high entropy alloy

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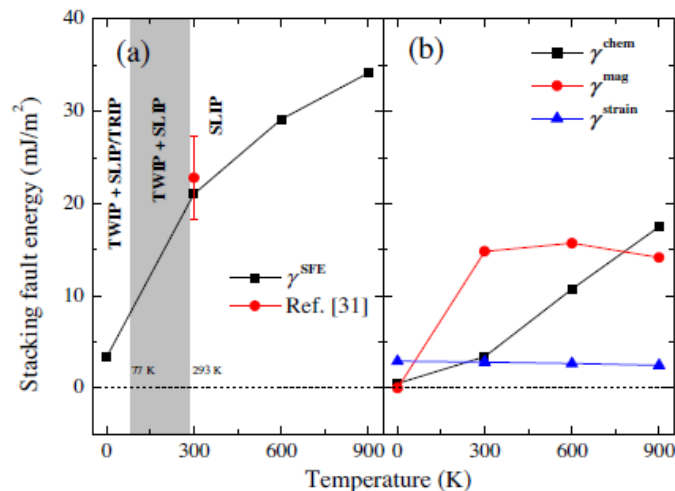
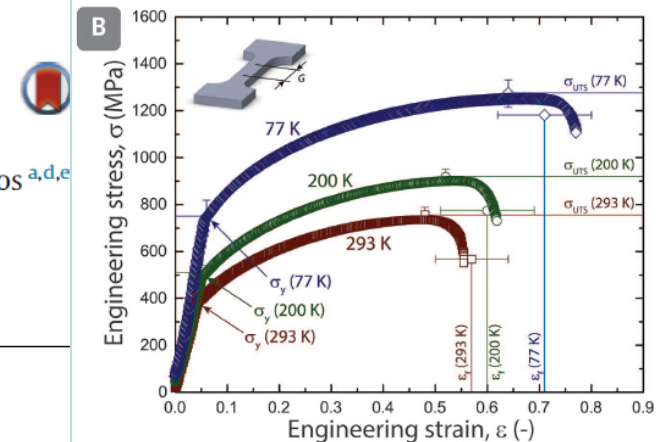
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## A fracture-resistant high-entropy alloy for cryogenic applications

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High-entropy alloys are equiatomic, multi-element systems that can crystallize as a single phase, despite containing multiple elements with different crystal structures. A rationale for this is that the configurational entropy contribution to the total free energy in alloys with five or more major elements may stabilize the solid-solution state relative to multiphase microstructures. We examined a five-element high-entropy alloy, CrMnFeCoNi, which forms a single-phase face-centered cubic solid solution, and found it to have exceptional damage tolerance with tensile strengths above 1 GPa and fracture toughness values exceeding 200 MPa·m<sup>1/2</sup>. Furthermore, its mechanical properties actually improve at cryogenic temperatures; we attribute this to a transition from planar-slip dislocation activity at room temperature to deformation by mechanical nanotwinning with decreasing temperature, which results in continuous steady strain hardening.

# Summary

- (1) EMTO-CPA reproduces well the experimentally observed values and trends of the structural and mechanical properties of ordered and random systems
- (2) special attention must be paid to the MT potential and single-site approximation

## Important features:

- Localized MT orbitals (similar to the screened KKR)
- Smooth energy dependence of  $S(\mathbf{e},\mathbf{k})$
- Optimized overlapping MT potential
- Proper normalization
- Accurate Full Charge Density
- Accurate kinetic and total energy